

2% 5V, 750mA Low Dropout Linear Regulator with Delayed RESET

Description

The CS-8122 is a precision 5V linear regulator capable of sourcing in excess of 750mA. The \overline{RESET} 's delay time is externally programmed using a discrete RC network. During power up, or when the output goes out of regulation, the RESET pin remains in the low state for the duration of the delay. This function is independent of the input voltage and will function correctly as long as the output voltage remains at or above 1V. Hysteresis is included in the delay and the RESET comparators to improve noise immunity. A latching discharge circuit is used to discharge the delay capacitor when it is triggered by a brief fault condition.

The regulator is protected against a variety of fault conditions: i.e. reverse battery, overvoltage, short circuit and thermal runaway conditions. The regulator is protected against voltage transients ranging from -50V to +40V. Short circuit current is limited to 1.2A (typ).

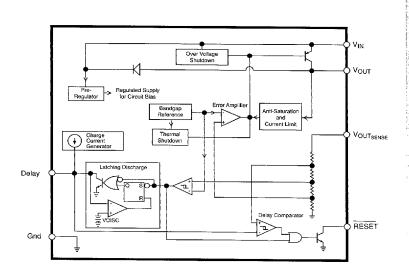
The CS-8122 is an improved replacement for the CS-8126 and features a tighter tolerance on its output voltage (2% vs 4%).

The CS-8122 is packaged in a 5 lead TO-220 with copper tab. The copper tab can be connected to a heat sink if necessary.

Features

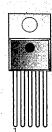
- 5V-t/-2% Regulated Output
- Low Dropout Voltage (0.6V @ 0.5A)
- 750mA Output Current Capability
- Externally Programmed RESET Delay
- Fault Protection
 Reverse Battery
 60V Load Dump
 -50V Reverse Transient
 Short Circuit
 Thermal Shutdown

Block Diagram



Package Options

5L TO-220



- 1 V_{IN}
- 2 V_{OUT}
- Gnd
- 1 Delay
- 5 RESET



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Absolute Maximum Ratings

Input Operating Range	—0.5 to 26V
Power Dissipation	Internally Limited
Transient Input Voltage	50V, 60V
Output Current	
ESD Susceptibility (Human Body Model)	
Operating Temperature	40°C to 125°C
Junction Temperature	
Storage Temperature	
Lead Temperature Soldering	
Wave Solder (through hole styles only)	10 sec. max, 260°C peak

Electrical Characteristics: -40°C \leq T_A \leq +125°C, -40°C \leq T_J \leq +150°C, 6V \leq V_{IN} \leq 26V, 5mA \leq I_{OUT} \leq 500mA, R_{RESET}=4.7k Ω to V_{CC} unless otherwise noted*

PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
■ Output Stage (V _{OUT})					
Output Voltage		4.9	5.0	5.1	V
Dropout Voltage	$I_{OUT} = 500 \text{mA}$		0.35	0.60	V
Supply Current	$I_{OUT} \le 10 \text{mA}$		2	7	mA
	$I_{OUT} \le 100 \text{mA}$		6	12	
	$I_{OUT} \le 500 \text{mA}$		55	100	
Line Regulation	$6V \le V_{JN} \le 26V$, $I_{OUT} = 50 \text{mA}$		5	50	mV
Load Regulation	$50 \text{mA} \le I_{\text{OUT}} \le 500 \text{mA}, V_{\text{IN}} = 14 \text{V}$		10	50	mV
Ripple Rejection	$\begin{split} f = &120 Hz, \ V_{IN} = 7, to \ 17V, \end{split}$ $I_{OUT} = &250 mA \end{split}$	54	75		dB
Current Limit		0.75	1.20		A
Overvoltage Shutdown		32		40	V
Maximum Line Transient	$V_{OUT} \le 5.5V$	60	95		V
Reverse Polarity Input Voltage DC	$V_{out} \ge -0.6V$, $10\Omega Load$	-15	-30		V
Reverse Polarity Input Voltage Transient	1% Duty Cycle, T < 100ms, 10Ω Load	-50	-80		

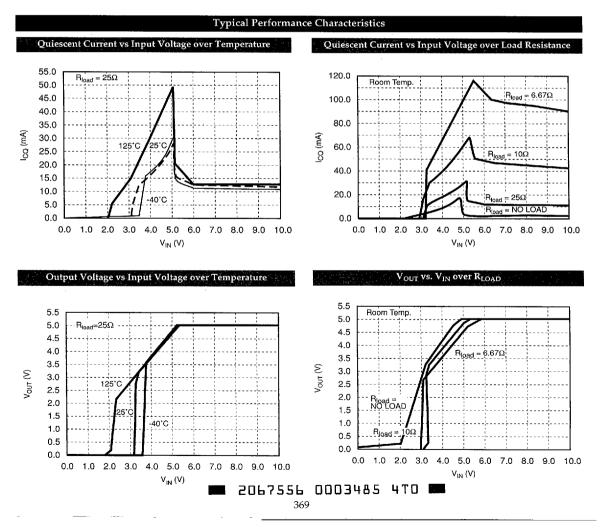
RESET and Delay Function	3				
Delay Charge Current	$V_{DELAY} = 2V$	5	10	15	μΑ
RESET Threshold	V _{OUT} Increasing, V _{RTON} V _{OUT} Decreasing, V _{RTOFF}	4.65 4.50	4.90 4.70	V _{OUT} -0.01 V _{OUT} -0.16	E BERTHROOM TRANSPORTER
RESET Hysteresis	$V_{RH} = V_{RT_{ON}} - V_{RT_{OFF}}$	150	200	250	mV
Delay Threshold	Charge, V _{DCHI} Discharge, V _{DCLOW}	3.25 2.85	3.50 3.10	3.75 3.35	V V
Delay Hysteresis		200	400	800	mV
RESET Output Voltage Low	$1V\!<\!V_{OUT}\!<\!V_{RTL}$ 3k $\!\Omega$ to V_{OUT}		0.1	0.4	\mathbf{v}
RESET Output Leakage Current	$V_{OUT} > V_{RTH}$		0	10	μΑ
Delay Capacitor Discharge Voltage	Discharge Latched "ON", V _{OUT} > V _{RT}		0:2	0.5	V
Delay Time	$C_{DELAY} = 0.1 \mu F$	16	32	48	ms

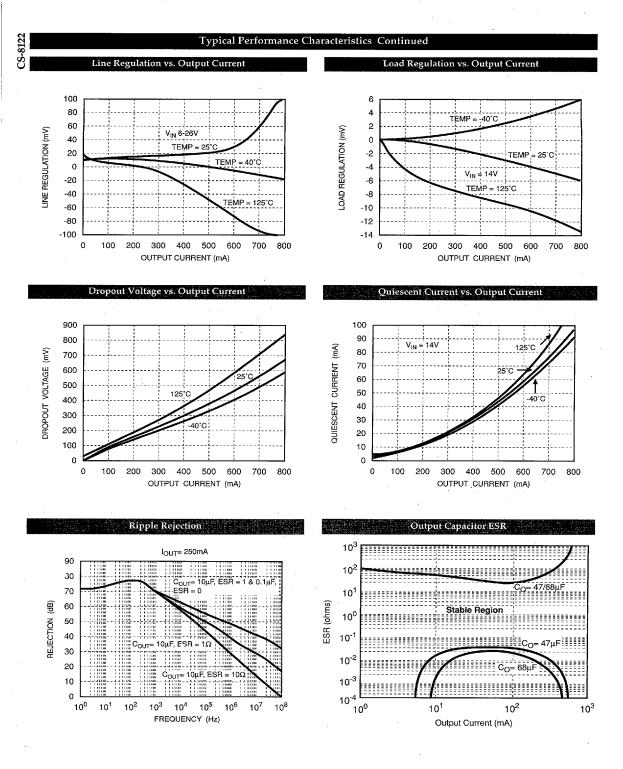
^{*} To observe safe operating junction temperatures, low duty cycle pulse testing is used in tests where applicable.

 $Delay\ Time = \frac{C_{Delay} \times V_{Delay\ Threshold\ Charge}}{L_{Course}} = C_{Delay} \times 3.5 \times 10^5 (typ)$

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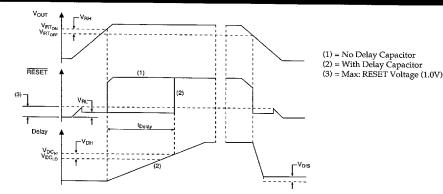
Package Pin Description			
PACKAGE PIN # 5L TO-220	PIN SYMBOL	• FUNCTION	
 1	V _{IN}	Unregulated supply voltage to IC.	
2	V _{OUT}	Regulated 5V output.	
3	Gnd	Ground connection.	
4	Delay	Timing capacitor for RESET function.	
5	RESET	CMOS/TTL compatible output pin. $\overline{\text{RESET}}$ goes low whenever V_{OUT} drops below 6% of it's regulated value.	





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(2) = With Delay Capacitor



Circuit Description

The CS-8122 RESET function, has hysteresis on both the Reset and Delay comparators, a latching Delay capacitor discharge circuit, and operates down to 1V.

The RESET circuit output is an open collector type with ON and OFF parameters as specified. The RESET output NPN transistor is controlled by the two circuits described (see Block Diagram).

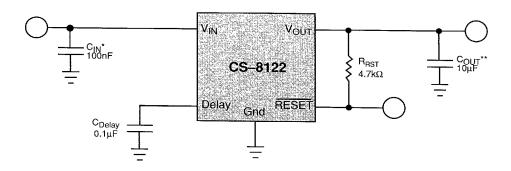
Low Voltage Inhibit Circuit

The Low Voltage Inhibit Circuit monitors output voltage, and when output voltage is below the specified minimum, causes the RESET output transistor to be in the ON (saturation) state. When the output voltage is above the specified level, this circuit permits the RESET output transistor to go into the OFF state if allowed by the RESET Delay circuit.

Reset Delay Circuit

The Reset Delay Circuit provides a programmable (by external capacitor) delay on the RESET output pin. The Delay pin provides source current to the external delay capacitor only when the Low Voltage Inhibit circuit indicates that output voltage is above $V_{\text{RT}_{\mbox{\scriptsize ON}}}$. Otherwise, the Delay pin sinks current to ground (used to discharge the delay capacitor). The discharge current is latched ON when the output voltage is below $V_{\text{RT}_{\mbox{OFF}'}}$ or when the voltage on the delay capacitor is above VDIS. The Delay capacitor is fully discharged anytime the output voltage falls out of regulation, even for a short period of time. This feature ensures that a controlled RESET pulse is generated following detection of an error condition. The circuit allows the RESET output transistor to go to the OFF (open) state only when the voltage on the Delay pin is higher than

Test Circuit



*C_{IN} required if regulator is far from power source filter.

**C_{OUT} required for stability.

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Stability Considerations

The output or compensation capacitor helps determine three main characteristics of a linear regulator: start-up delay, load transient response and loop stability.

The capacitor value and type should be based on cost, availability, size and temperature constraints. A tantalum or aluminum electrolytic capacitor is best, since a film or ceramic capacitor with almost zero ESR, can cause instability. The aluminum electrolytic capacitor is the cheapest solution, but, if the circuit operates at low temperatures (-25°C to -40°C), both the value and ESR of the capacitor will vary considerably. The capacitor manufacturers data sheet usually provide this information.

The value for the output capacitor C_{OUT} shown in the test and applications circuit should work for most applications, however it is not necessarily the best solution.

To determine an acceptable value for C_{OUT} for a particular application, start with a tantalum capacitor of the recommended value and work towards a less expensive alternative part.

Step 1: Place the completed circuit with a tantalum capacitor of the recommended value in an environmental chamber at the lowest specified operating temperature and monitor the outputs on the oscilloscope. A decade box connected in series with the capacitor will simulate the higher ESR of an aluminum capacitor.

(Leave the decade box outside the chamber, the small resistance added by the longer leads is negligible)

Step 2: With the input voltage at its maximum value, increase the load current slowly from zero to full load while observing the output for any oscillations. If no oscillations are observed, the capacitor is large enough to ensure a stable design under steady state conditions.

Step 3: Increase the ESR of the capacitor from zero using the decade box and vary the load current until oscillations appear. Record the values of load current and ESR that cause the greatest oscillation. This represents the worst case load conditions for the regulator at low temperature.

Step 4: Maintain the worst case load conditions set in step 3 and vary the input voltage until the oscillations increase. This point represents the worst case input voltage conditions.

Step 5: If the capacitor is adequate, repeat steps 3 and 4 with the next smaller valued capacitor. (A smaller capacitor will usually cost less and occupy less board space.) If the capacitor oscillates within the range of expected operating conditions, repeat steps 3 and 4 with the next larger standard capacitor value.

Step 6: Test the load transient response by switching in various loads at several frequencies to simulate its real work environment. Vary the ESR to reduce ringing.

Step 7: Remove the unit from the environmental chamber and heat the IC with a heat gun. Vary the load current as instructed in step 5 to test for any oscillations.

Once the minimum capacitor value with the maximum ESR is found, a safety factor should be added to allow for the tolerance of the capacitor and any variations in regulator performance. Most good quality aluminum electrolytic capacitors have a tolerance of \pm 20% so the minimum value found should be increased by at least 50% to allow

for this tolerance plus the variation which will occur at low temperatures. The ESR of the capacitor should be less than 50% of the maximum allowable ESR found in step 3 above.

Calculating Power Dissipation in a Single Output Linear Regulator

The maximum power dissipation for a single output regulator (Figure 1) is

$$P_{D(max)} = [V_{IN(max)} - V_{OUT(min)}]I_{OUT(max)} + V_{IN(max)}I_{Q}$$
 (1)

where

 $V_{\text{IN}(\text{max})}$ is the maximum input voltage,

V_{OUT(min)} is the minimum output voltage,

 $I_{OUT(max)}$ is the maximum output current, for the application

 I_Q is the quiescent current the regulator consumes at $I_{\text{OUT}(\text{max})}$

Once the value of $P_{D(max)}$ is known, the maximum permissible value of $R\Theta_{JA}$ can be calculated:

$$R\Theta_{JA} = \frac{150^{\circ}C - T_{A}}{P_{D}}$$
 (2)

The value of $R\Theta_{JA}$ can then be compared with those in the package section of the data sheet. Those packages with $R\Theta_{JA}$'s less than the calculated value in equation 2 will keep the die temperature below 150°C.

In some cases, none of the packages will be sufficient to dissipate the heat generated by the IC, and an external heatsink will be required.

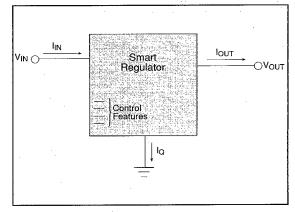


Figure 1: Single output regulator with key performance parameters labeled.

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Application Notes: continued

Heat Sinks

A heat sink effectively increases the surface area of the package to improve the flow of heat away from the IC and into the surrounding air.

Each material in the heat flow path between the IC and the outside environment will have a thermal resistance. Like series electrical resistances, these resistances are summed to determine the value of $R\Theta_{IA}$.

$$R\Theta_{JA} = R\Theta_{JC} + R\Theta_{CS} + R\Theta_{SA}$$
 (3)

where

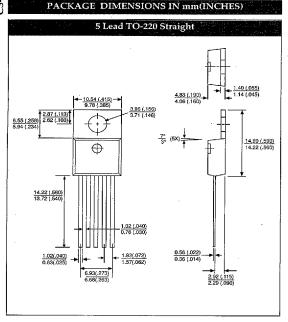
 $R\Theta_{IC}$ = the junction–to–case thermal resistance,

 $R\Theta_{CS}$ = the case—to—heatsink thermal resistance, and

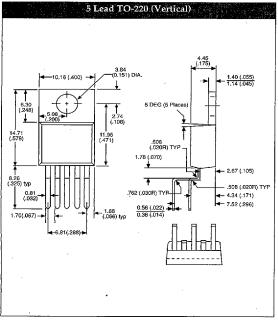
 $R\Theta_{SA}$ = the heatsink–to–ambient thermal resistance.

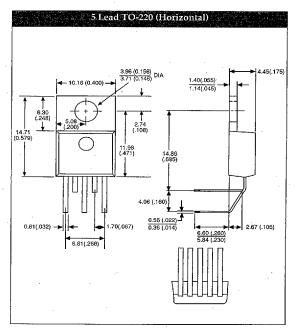
 $R\Theta_{JC}$ appears in the package section of the data sheet. Like $R\Theta_{JA}$, it too is a function of package type. $R\Theta_{CS}$ and $R\Theta_{SA}$ are functions of the package type, heatsink and the interface between them. These values appear in heat sink data sheets of heat sink manufacturers.





PACKAGE THERMAL DATA				
Therma	l Data	TO-220		
$R\Theta_{JC}$	typ	3.5	°C/W	
RΘ _{JA}	typ	50	°C/W	





Ordering Information		
Part Number	Description	
CS-8122T5	5L TO-220 Straight	
CS-8122TH5	5L TO-220 Horizontal	
CS-8122TV5	5L TO-220 Vertical	

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