

The A3250 and A3251 are field-programmable, chopper-stabilized, unipolar Halleffect switches designed for use in high-temperature applications. These devices use a chopper-stabilization technique to eliminate offset inherent in single-element devices.

The A3250 and A3251 are externally programmable devices. The devices have a wide range of programmability of the magnetic operate point (B_{OP}) while the hysteresis remains fixed. This advanced feature allows for optimization of the sensor switchpoint and can drastically reduce the effects of variations found in a production environment, such as magnet and device placement tolerances.

These devices provide on-chip transient protection. A Zener clamp on the power supply protects against overvoltage conditions on the supply line. These devices also include short-circuit protection on the output.

The output of the A3250 switches LOW when subjected to a south-polarity magnetic field with a flux density that exceeds the threshold for B_{OP} , and switches HIGH when the field drops below the magnetic release point, B_{RP} . The output of the A3251 has the opposite polarity, switching HIGH in a south-polarity magnetic field that B_{OP} , and switching LOW when the field drops below B_{RP} .

The other differences in the devices are the power-on state. The A3250 powers-on in the HIGH state, while the A3251 powers-on in the LOW state.

These devices are available in a TO-92 three-lead ultra-mini SIP (Single In-line Package), with either straight or formed and trimmed lead configuration.

Features and Benefits

- Chopper stabilization for stable switchpoints throughout operating temperature range
- Externally programmable operate point (through VCC pin)
- On-chip protection against:
 Supply transients
 - Output short-circuits
 - Reverse-battery condition
- On-board voltage regulator for 4.2 V to 24 V operation

Use the following complete part numbers when ordering:

Port Number	Paakaga	T _A	B _{hys(typ)}	V _{out}		
Falt Nulliber	Fackage	(°C)	(G)	Power-On	Running*	
A3250JUA A3250JUATL	Straight lead Formed lead	-40 to 115	18	High	Low	
A3250LUA A3250LUATL	Straight lead Formed lead	–40 to 150	13	підп		
A3251JUA A3251JUATL	Straight lead Formed lead	-40 to 115	18	Low	High	
A3251LUA A3251LUATL	Straight lead Formed lead	-40 to 150	13	LOW		

*In south polarity magnetic field of sufficient strength.





ABSOLUTE MAXIMUM RATINGS

Supply Voltage, V _{CC}	
Reverse-Supply Voltage, V _{RCC}	–18 V
Zener Overvoltage, V _Z	
Output Current, I _{OUT}	20 mA
Magnetic Flux Density, B	Unlimited
Operating Temperature	
Ambient, T _A , Range J	40°C to 115°C
Ambient, T _A , Range L	40°C to 150°C
Maximum Junction, T _{I(max)}	165°C
Storage Temperature, T _S	65°C to 170°C

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Functional Block Diagram



Hysteresis Curves

A3250



Output voltage in relation to sensed magnetic flux density in a south polarity magnetic field of sufficient strength. Transition through B_{OP} must precede transition through B_{RP} .



A3251

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OPERATING CHARACTERISTICS valid over operating T _A and V _{CC} , unless otherwise specified								
Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units		
ELECTRICAL CHARACTERIST	ICS		•					
Supply Voltage ¹	V _{CC}	Running mode	4.2	-	24	V		
Output Saturation Voltage	V _{OUT(sat)}	I _{OUT} = 20 mA; Switch state = ON	-	175	400	mV		
Output Leakage Current	I _{OFF}	V _{OUT} = 24 V; Switch state = OFF	-	-	10	μA		
	I _{CC(off)}	A3250; B <b<sub>RP; V_{OUT} = HIGH</b<sub>	_	4.0	7.0	mA		
Cumply Cumpat		A3251; B>B _{OP} ; V _{OUT} = HIGH	-	4.0	7.0	mA		
Supply Current	I _{CC(on)}	A3250; B>B _{OP} ; V _{OUT} = LOW	-	6.0	10.0	mA		
		A3251; B <b<sub>RP; V_{OUT} = LOW</b<sub>	_	6.0	10.0	mA		
Output Rise Time	t _r	R_{LOAD} = 820 Ω, C_{LOAD} = 10 pF	-	-	5.0	μs		
Output Fall Time	t _f	R_{LOAD} = 820 Ω, C_{LOAD} = 10 pF	-	_	5.0	μs		
Chopping Frequency	f _C		-	340	-	kHz		
Power-Up Time	t _{on}	V _{OUT} = HIGH	-	20	50	μs		
Output Current Limit ^{1,2}	I _{OUT(lim)}	Short-circuit protection	60	90	120	mA		
	POS	A3250; B < B _{RP} , t > t _{on}	_	HIGH	_	mV		
Power-On State		A3251; B < B _{RP} , t > t _{on}	-	LOW	_	mV		
MAGNETIC CHARACTERISTIC	S		I	1	I	I		
Initial Operate Point	B _{OP}		-20	13	50	G		
Temperature Drift of B _{OP}	ΔΒ _{ΟΡ}	B _{OP} ≤ 500 gauss	-35	_	35	G		
	B _{hys}	Package T _A range = J	5.0	18	35	G		
Hysteresis (B _{OP} – B _{RP})		Package T _A range = L	5.0	13	35	G		
PROGRAMMING CHARACTER	ISTICS					1		
Programmable B _{OP} Values ³	B _{OP(prog)}		50	-	≥350	G		
	_	Switchpoint set	_	6	_	Bit		
Number of Programming Bits		Programming lock	_	1	_	Bit		
Resolution	B _{RES}		_	7.0	_	G		
TRANSIENT PROTECTION CH	ARACTERIST	ics			I	1		
Supply Zener Voltage	Vz		28	-	_	V		
Supply Zener Current	Ι _Ζ	V _{CC} = 28 V	-	-	13	mA		
Reverse Battery Current	I _{RCC}	V_{RCC} = -18 V, T_{J} < $T_{J(max)}$	-	-	-5.0	mA		

¹ Do not exceed TJ(max): Additional information on power derating is provided in the applications section.

² Short-circuit protection is not intended for continuous operation; permanent damage may result.

³ Device can be used below 50 G but is not guaranteed to be a unipolar switch. It is the responsibility of the programmer to verify that the desired switchpoint has been achieved.



Field-Programmable, Chopper-Stabilized, Unipolar Hall-Effect Switches

Typical Characterization Data

All data are taken with A3250 devices, the average of 3 lots, 30 pieces per lot





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THERMAL CHARACTERISTICS may require derating at maximum conditions, see application information

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max	Units
Package Thermal Resistance	$R_{\theta JA}$	Package UA, minimum-K PCB (single-sided with copper limited to solder pads)	165	_	_	°C/W







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Functional Description

Chopper-Stabilized Technique

The Hall sensor is based on a Hall element, a small sheet of semiconductor material in which a constant bias current flows when a constant voltage source is applied. The output takes the form of a voltage measured across the width of the Hall element, and has negligible value in the absence of a magnetic field. When a magnetic field is applied with flux lines at right angles to the current in the Hall element, a small signal voltage directly proportional to the strength of the magnetic field occurs at the output of the Hall element.

This small signal voltage is disproportionally small relative to the offset produced at the input of the device. This makes it very difficult to process the signal and maintain an accurate, reliable output over the specified temperature and voltage range. Therefore, it is important to reduce any distortion of the signal that could be amplified when the signal is processed.

Chopper stabilization is a unique approach used to minimize input offset on the Hall IC. This technique removes a key source of output drift due to temperature and mechanical stress, and produces a 3X reduction in offset in comparison to other, conventional methods.

This offset reduction chopping technique is based on a signal modulation-demodulation process. The undesired offset signal is separated from the magnetically-induced signal in the frequency domain. The offset (and any low-frequency noise) component of the signal can be seen as signal distortion added after the signal modulation process has taken place. Therefore, the dc offset is not modulated and remains a low-frequency component. Consequently, the signal demodulation process acts as a modulation process for the offset, causing the magnetically-induced signal to recover its original spectrum at baseband while the dc offset becomes a high-frequency signal. Then, the signal passes using a low-pass filter, while the modulated dc offset is suppressed.

The advantage of this approach is significant offset reduction, which desensitizes the Hall IC against the effects of temperature and mechanical stress. The disadvantage is that this technique features a demodulator that uses a sample-and-hold block to store and recover the signal. This sampling process can slightly degrade the SNR (signal-to-noise ratio) by producing replicas of the noise spectrum at the baseband. This degradation is a function of the ratio between the white noise spectrum and the sampling frequency. The effect of the degradation of the SNR is higher jitter, also known as signal repeatability. However, the jitter in a continuous-time device can be 5X that of the A3250/A3251.



Chopper stabilization circuit (dynamic quadrature offset cancellation)



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Programming Protocol

The operate switchpoint, B_{OP} , can be field-programmed. To do so, a coded series of voltage pulses through the VCC pin is used to set bitfields in onboard registers. The effect on the device output can be monitored, and the registers can be cleared and set repeatedly until the required B_{OP} is achieved. To make the setting permanent, bitfield-level solid state fuses are blown, and finally, a device-level fuse is blown, blocking any further coding. It is not necessary to program the release switchpoint, B_{RP} , because the difference between B_{OP} and B_{RP} , referred to as the hysteresis, B_{HYS} , is fixed.

The range of values between $B_{OP(min)}$ and $B_{OP(max)}$ is scaled to 64 increments. The actual change in magnetic flux (G) represented by each increment is indicated by B_{RES} (see the Operating Characteristics table; however, testing is the only method for verifying the resulting B_{OP}). For programming, the 64 increments are individually identified using 6 data bits, which are physically represented by 6 bitfields in the onboard registers. By setting these bitfields, the corresponding calibration value is programmed into the device.

Three voltage levels are used in programming the device: a low voltage, V_{PL} , a minimum required to sustain register settings; a mid-level voltage, V_{PM} , used to increment the address counter in the device; and a high voltage, V_{PH} , used to separate sets of V_{PM} pulses (when short in duration) and to blow fuses (when long in duration). A fourth voltage level, essentially 0 V, is used to clear the registers between pulse sequences. The pulse values are shown in the Programming Protocol Characteristics table and in figure 1.



Figure 1. Pulse amplitudes and durations

Additional information on device programming and programming products is available on www. allegromicro.com. Programming hardware is available for purchase, and programming software is available free of charge.

Code Programming. Each bitfield must be individually set. To do so, a pulse sequence must be transmitted for each bitfield that is being set to 1. If more than one bitfield is being set to 1, all pulse sequences must be sent, one after the other, without allowing V_{CC} to fall to zero (which clears the registers).

The same pulse sequence is used to provisionally set bitfields as is used to permanently set bitfield-level fuses. The only difference is that when provisionally setting bitfields, no fuse-blowing pulse is sent at the end of the pulse sequence.

Characteristic	Symbol	Test Conditions	Min.	Тур.	Max.	Units
Programming Voltage ¹ Programming Current ²	V _{PL}	Minimum voltage range during programming	4.5	5.0	5.5	V
	V _{PM}		10	11	12	V
	V _{PH}		23	25	26	V
Programming Current ²	I _{PP}	Maximum supply current during programming	_	500	_	mA
Pulse Width	t _{d(0)}	OFF time between programming bits	20	_	-	μs
	t _{d(1)}	Pulse duration (ON time) for enable, address, fuse blowing or lock bits	20	_	_	μs
	t _{d(P)}	Pulse duration (ON time) for fuse blowing	100	300	-	μs
Pulse Rise Time	t _r	V_{PL} to V_{PM} ; V_{PL} to V_{PH}	11	_	_	μs
Pulse Fall Time	t _f	V_{PM} to V_{PL} ; V_{PH} to V_{PL}	5	_	_	μs

PROGRAMMING PROTOCOL CHARACTERISTICS, T_A = 25°C, unless otherwise noted

¹Programming voltages are measured at the VCC pin.

²A bypass capacitor with a minimum capacitance of 0.1 µF must be connected from VCC to the GND pin of the device in order to provide the current necessary to blow the fuse.



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The pulse sequences consist of the following groups of pulses:

- 1. An enable sequence.
- 2. A bitfield address sequence.
- 3. When permanently setting the bitfield, a long V_{PH} fuse-blowing pulse. (Note: Blown bit fuses cannot be reset.) When provisionally trying a value, a short V_{PH} pulse.
- 4. When permanently setting the bitfield, the level of V_{CC} must be allowed to drop to zero between each pulse sequence, in order to clear all registers. However, when provisionally setting bitfields, V_{CC} must be maintained at V_{PL} between pulse sequences, in order to maintain the prior bitfield settings while preparing to set additional bitfields.

Bitfields that are not set are evaluated as zeros. The bitfield-level

fuses for 0 value bitfields are never blown. This prevents inadvertently setting the bitfield to 1. Instead, blowing the devicelevel fuse protects the 0 bitfields from being accidentally set in the future.

Two pulse sequences for provisionally trying the calibration value 5 are shown in figure 2. Because the bitfields must be set individually, 5_{10} must be programmed as binary 101. Bit 3 is set to 1 (000100₂, which is 4_{10}), then bit 1 is set to 1 (000001₂, which is 1_{10}). Bit 2 is ignored, and so remains 0.

Two pulse sequences for permanently setting the calibration value 5 are shown in figure 3. The final V_{PH} pulse, which was used as a short delimiter when trying values, is maintained for a longer period, enough to blow the corresponding bitfield-level fuse.



Figure 2. Pulse sequence to provisionally try calibration value 5 (101 binary, or bitfield address 3 and bitfield address 1).



Figure 3. Pulse sequence to permanently encode calibration value 5 (101 binary, or bitfield address 3 and bitfield address 1).



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Enabling Addressing Mode. The first segment of code is a keying sequence used to enable the bitfield addressing mode. As shown in figure 4, this segment consists of one short V_{PH} pulse, seven or more V_{PM} pulses, and one V_{PH} pulse, with no supply interruptions. This sequence is designed to prevent the device from being programmed accidentally, such as by noise on the supply line.



Figure 4. Addressing mode enable pulse sequence

Address Selection. After addressing mode is enabled, the

Lock Bit Programming. After the desired B_{OP} calibration value is programmed, and all of the corresponding bitfield-level fuses

are blown, the device-level fuse should be blown. To do so, the lock bit (bitfield address 65) should be encoded as 1 and have

its fuse blown. This is done in the same manner as permanently

setting the other bitfields, as shown in figure 6.



Figure 5. Pulse sequence to select addresses



Figure 6. Pulse sequence to encode lock bit



target bitfield address, is indicated by a series of VPM pulses, as shown in figure 3. When provisionally trying a value, this sequence is followed by a short V_{PH} pulse, which serves to delimit the address and set the corresponding bitfield. When permanently setting a bitfield, the VPH pulse is continued for a longer period of time, suffienct to not only set the bitfield to 1, but also to blow the bitfield fuse.

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Application Information

For additional general application information, visit the Allegro MicroSystems Web site at www. allegromicro.com.

Typical Application Circuit

It is strongly recommended that an external ceramic bypass capacitor, C_{BYP} , in the range of 0.01 µF to 0.1 µF be connected between the VCC pin and the supply and GND pin to reduce both external noise and noise generated by the chopper-stabilization technique. (The diagram at the right shows C_{BYP} at 0.1 µF.) C_{BYP} should be installed so that the traces that connect it to the A3250/A3251 are no greater than 5 mm in length.

The series resistor R_S , in combination with C_{BYP} creates a filter for EMI pulses. (Additional information on EMC is provided on the Allegro MicroSystems Web site.) R_S will have a drop of approximately 800 mV. This must be taken into consideration when determining the minimum VCC requirement for the A3250/A3251. The pull-up resistor, R_L , should be chosen to limit the current through the output transistor; do not exceed the maximum continuous output current of the device.



Typical application circuit



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Power Derating

The device must be operated below the maximum junction temperature of the device, $T_{J(max)}$. Under certain combinations of peak conditions, reliable operation may require derating supplied power or improving the heat dissipation properties of the application. This section presents a procedure for correlating factors affecting operating T_J . (Thermal data is also available on the Allegro MicroSystems Web site.)

The Package Thermal Resistance, $R_{\theta JA}$, is a figure of merit summarizing the ability of the application and the device to dissipate heat from the junction (die), through all paths to the ambient air. Its primary component is the Effective Thermal Conductivity, K, of the printed circuit board, including adjacent devices and traces. Radiation from the die through the device case, $R_{\theta JC}$, is relatively small component of $R_{\theta JA}$. Ambient air temperature, T_A , and air motion are significant external factors, damped by overmolding.

The effect of varying power levels (Power Dissipation, P_D), can be estimated. The following formulas represent the fundamental relationships used to estimate T_J , at P_D .

$$P_{D} = V_{IN} \times I_{IN}$$
(1)
$$\Delta T = P_{D} \times R_{\theta JA}$$
(2)
$$T_{I} = T_{A} + \Delta T$$
(3)

For example, given common conditions such as: $T_A = 25^{\circ}C$, $V_{CC} = 12 \text{ V}$, $I_{CC} = 4 \text{ mA}$, and $R_{\theta JA} = 165 ^{\circ}C/W$, then:

$$P_D = V_{CC} \times I_{CC} = 12 \text{ V} \times 4 \text{ mA} = 48 \text{ mW}$$

$$\Delta T = P_D \times R_{\Theta IA} = 48 \text{ mW} \times 165 \text{ }^{\circ}\text{C/W} = 8^{\circ}\text{C}$$

$$T_{I} = T_{A} + \Delta T = 25^{\circ}C + 8^{\circ}C = 33^{\circ}C$$

A worst-case estimate, $P_{D(max)}$, represents the maximum allowable power level ($V_{CC(max)}$, $I_{CC(max)}$), without exceeding $T_{J(max)}$, at a selected $R_{\theta JA}$ and T_A . *Example*: Reliability for V_{CC} at $T_A=150^{\circ}$ C, package UA, using minimum-K PCB.

Observe the worst-case ratings for the device, specifically: $R_{\theta JA}=165^{\circ}C/W$, $T_{J(max)}=165^{\circ}C$, $V_{CC(max)}=24$ V, and $I_{CC(max)}=10$ mA.

Calculate the maximum allowable power level, $P_{D(max)}$. First, invert equation 3:

$$\Delta T_{max} = T_{J(max)} - T_A = 165 \text{°C} - 150 \text{°C} = 15 \text{°C}$$

This provides the allowable increase to T_J resulting from internal power dissipation. Then, invert equation 2:

$$P_{D(max)} = \Delta T_{max} \div R_{\theta JA} = 15^{\circ}C \div 165^{\circ}C/W = 91 \text{ mW}$$

Finally, invert equation 1 with respect to voltage:

$$V_{CC(est)} = P_{D(max)} \div I_{CC(max)} = 91 \text{ mW} \div 10 \text{ mA} = 9 \text{ V}$$

The result indicates that, at T_A , the application and device can dissipate adequate amounts of heat at voltages $\leq V_{CC(est)}$.

Compare $V_{CC(est)}$ to $V_{CC(max)}$. If $V_{CC(est)} \leq V_{CC(max)}$, then reliable operation between $V_{CC(est)}$ and $V_{CC(max)}$ requires enhanced $R_{\theta JA}$. If $V_{CC(est)} \geq V_{CC(max)}$, then operation between $V_{CC(est)}$ and $V_{CC(max)}$ is reliable under these conditions.



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Package UA, 3-Pin; (TO-92)



The products described herein are manufactured under one or more of the following U.S. patents: 5,045,920; 5,264,783; 5,442,283; 5,389,889; 5,581,179; 5,517,112; 5,619,137; 5,621,319; 5,650,719; 5,686,894; 5,694,038; 5,729,130; 5,917,320; and other patents pending.

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