

MicroStar BGA™ Packaging Reference Guide

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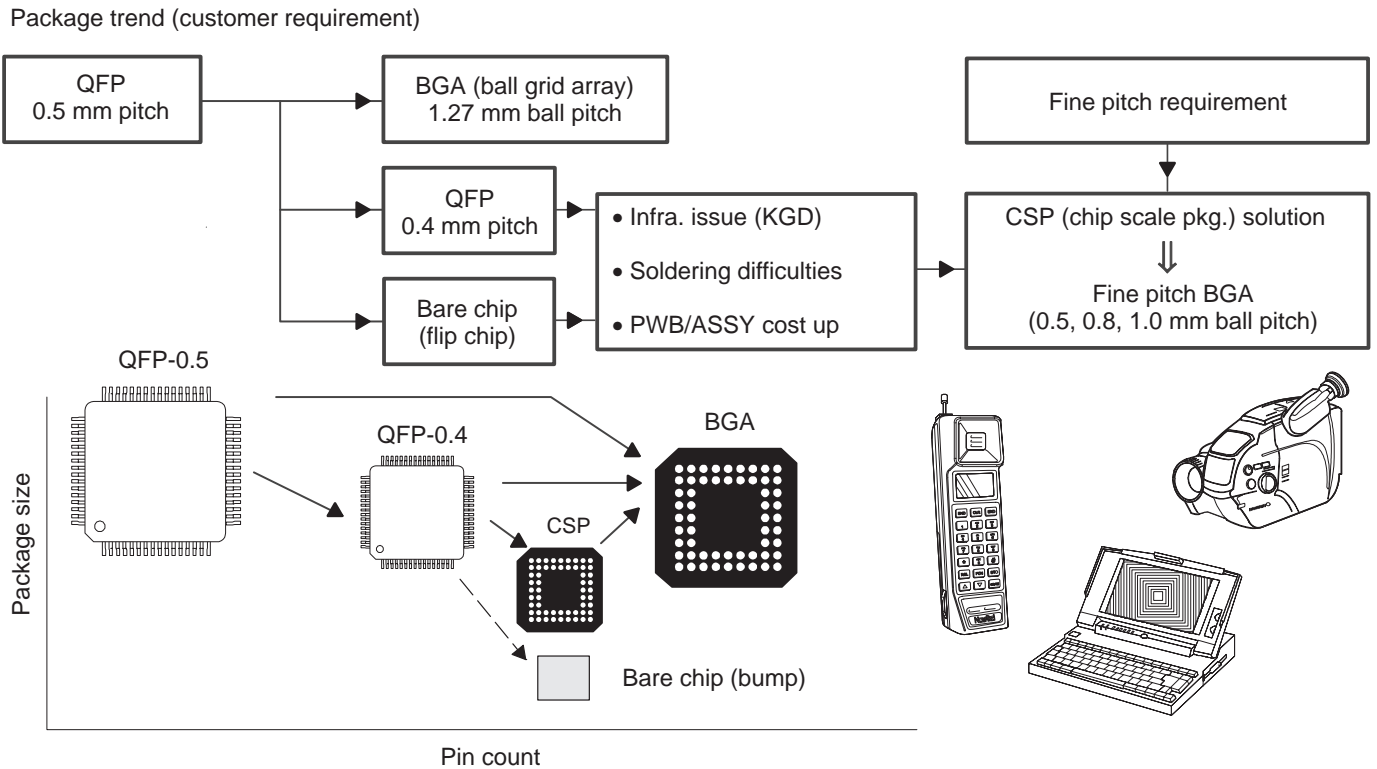
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Introduction

The parallel pursuit of cost reduction and miniaturization in recent years has given rise to an increasing emphasis on very small integrated circuit (IC) package solutions. This is particularly evident in consumer-based end

equipment using digital signal processor (DSP) solutions such as wireless telephones, laptop computers, and hard-disk drives. Despite the formal definition, packages with an area similar in size to the IC they encapsulate are loosely referred to as chip scale packages (CSPs). Figure 1 illustrates this trend.

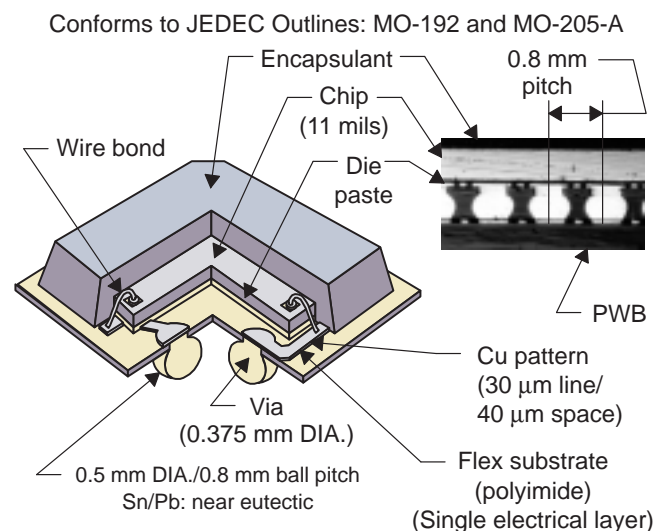
Figure 1. Packaging Trends



Chip scale packages are in many ways an ideal solution to the cost reduction and miniaturization requirements. They offer enormous area reductions in comparison to quad flat packages (QFPs) and have increasing potential to do so without adding to system-level cost. In the best case, CSPs compete today on a cost-per-terminal basis with QFPs. For example, various CSPs from Texas Instruments (TI™) are now available at cost parity with thin QFPs.

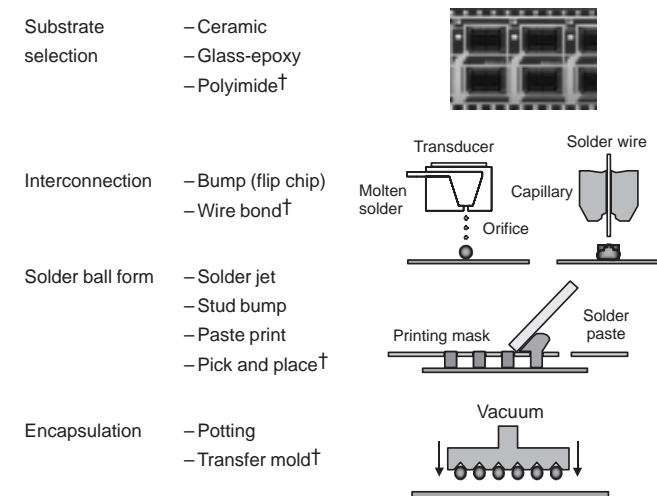
Texas Instruments produces a polyimide film-based family of CSPs called MicroStar BGA™. Like most other CSPs, MicroStar BGAs use solder alloy balls as the interconnect between the package substrate and the board on which the package is soldered. The MicroStar BGA family comes in a range of solder ball pitch (0.5 mm, 0.8 mm, and 1.0 mm). Currently, TI's most popular packages are 64- and 144-ball packages. Figure 2 shows the structure of TI's MicroStar BGA package.

Figure 2. Structure of TI's MicroStar BGA



Texas Instruments addressed several key issues in package assembly in order to produce a CSP that is not only physically and mechanically stable but cost-effective for a wide variety of applications. Figure 3 demonstrates how MicroStar BGAs resolve reliability and cost issues. An overall view of the flow used to produce TI MicroStar BGA packages is shown in Figure 4. The process for solder ball attachment is shown in Figure 5.

Figure 3. MicroStar BGA Package Assembly Issues



†These are the processes used by TI.

Figure 4. MicroStar BGA Package Assembly Flow

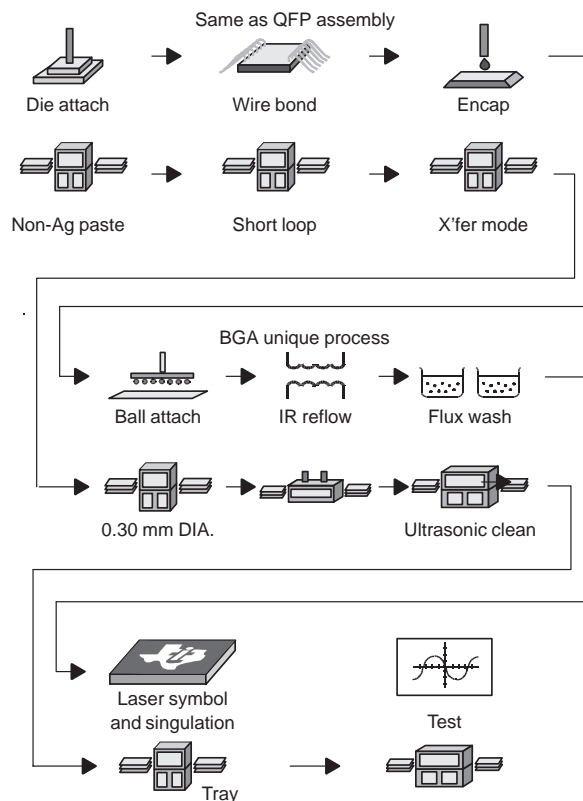
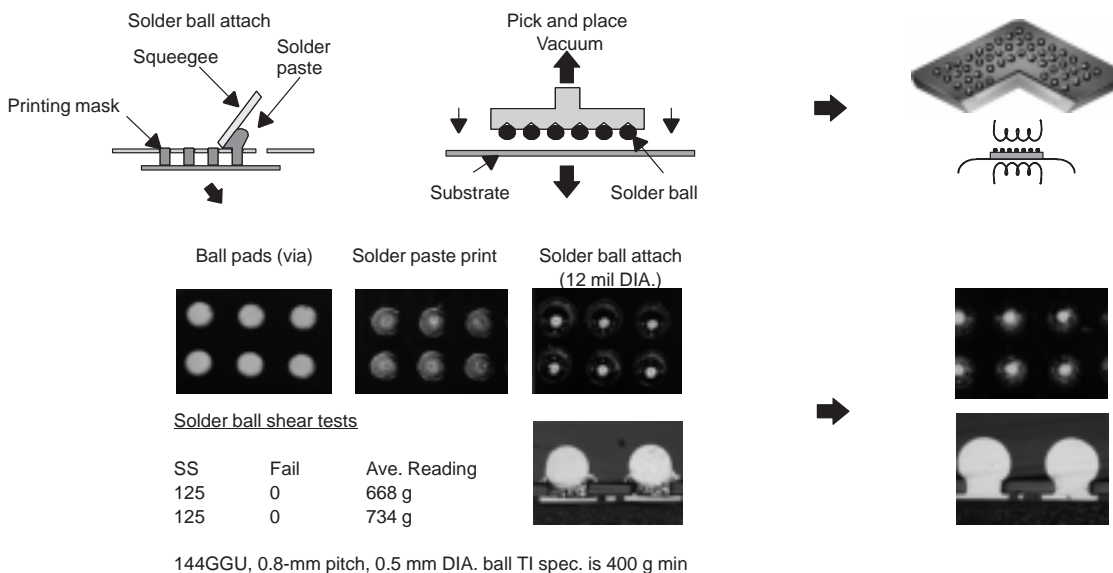


Figure 5. Solder Ball Attachment



Texas Instruments has qualified many product lines using the MicroStar BGA packages, and has now shipped more than 70 million production units. This guide is designed to give you technical background on MicroStar BGA packages as well as how they can be used to build advanced board layouts.

If you would like more information on using reliable and cost-effective MicroStar BGA packaging in your design, please contact your local TI field sales office.

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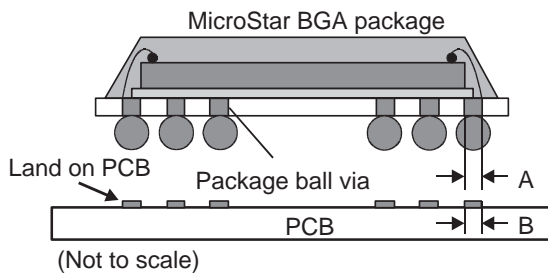
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PCB Design Considerations

Solder Land Areas

Design of both the MicroStar BGA itself and the printed circuit board (PCB) are important in achieving good manufacturability and optimum reliability. In particular, the diameters of the package vias and the board lands are critical. While the actual sizes of these dimensions are important, their ratio is more critical. Figure 6 illustrates the package via-to-PCB configuration and Figure 7 illustrates why this ratio is critical.

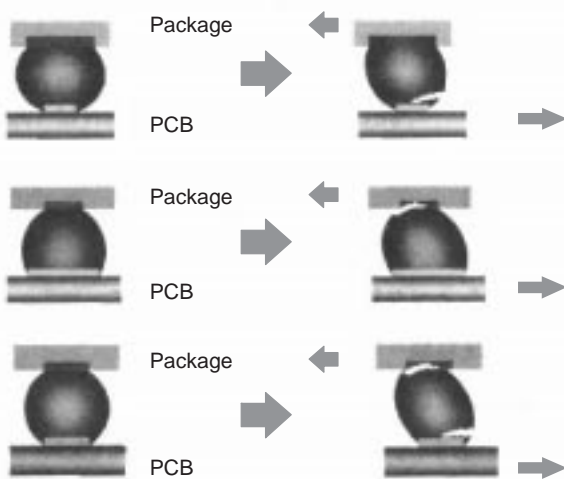
Figure 6. Package Via to Board Land Area Configuration



A = Via diameter on package
B = Land diameter on PCB

Ratio A/B should equal 1.0 for optimum reliability.

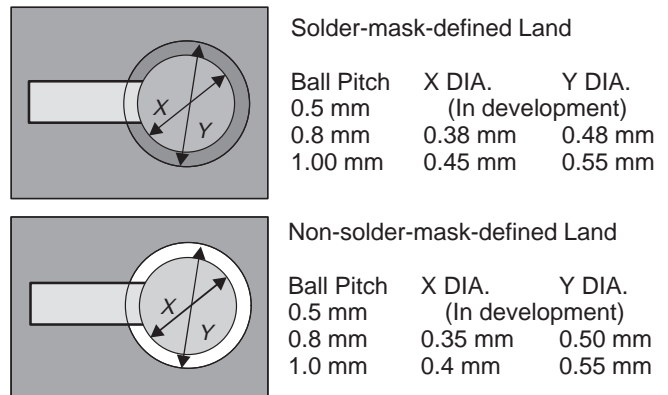
Figure 7. Effects of Via-to-Land Ratios



In the top view of Figure 7, the package via is larger than the PCB via, and the solder ball is prone to crack prematurely at the PCB interface. In the middle view, the PCB via is larger than the package via, which leads to cracks at the package surface. In the bottom view, where the ratio is almost 1:1, the stresses are equalized and neither site is more susceptible to cracking than the other.

Solder lands on the PCB are generally simple round pads. Solder lands are either solder-mask-defined or non-solder-mask-defined.

Figure 8. Optimum Land Configurations



Solder-mask-defined (SMD) land. With this method, the copper pad is made larger than the desired land area, and the opening size is defined by the opening in the solder mask material. The advantages normally associated with this technique include more closely controlled size and better copper adhesion to the laminate. Better size control is the result of photoimaging the stencils for masks. The chief disadvantage of this method is that the larger copper spot can make routing more difficult.

Non-solder-mask-defined (NSMD) land. Here, the land area is etched inside the solder mask area. While the size control is dependent on copper etching and is not as accurate as the solder mask method, the overall pattern registration is dependent on the copper artwork, which is quite accurate. The tradeoff is between accurate dot placement and accurate dot size.

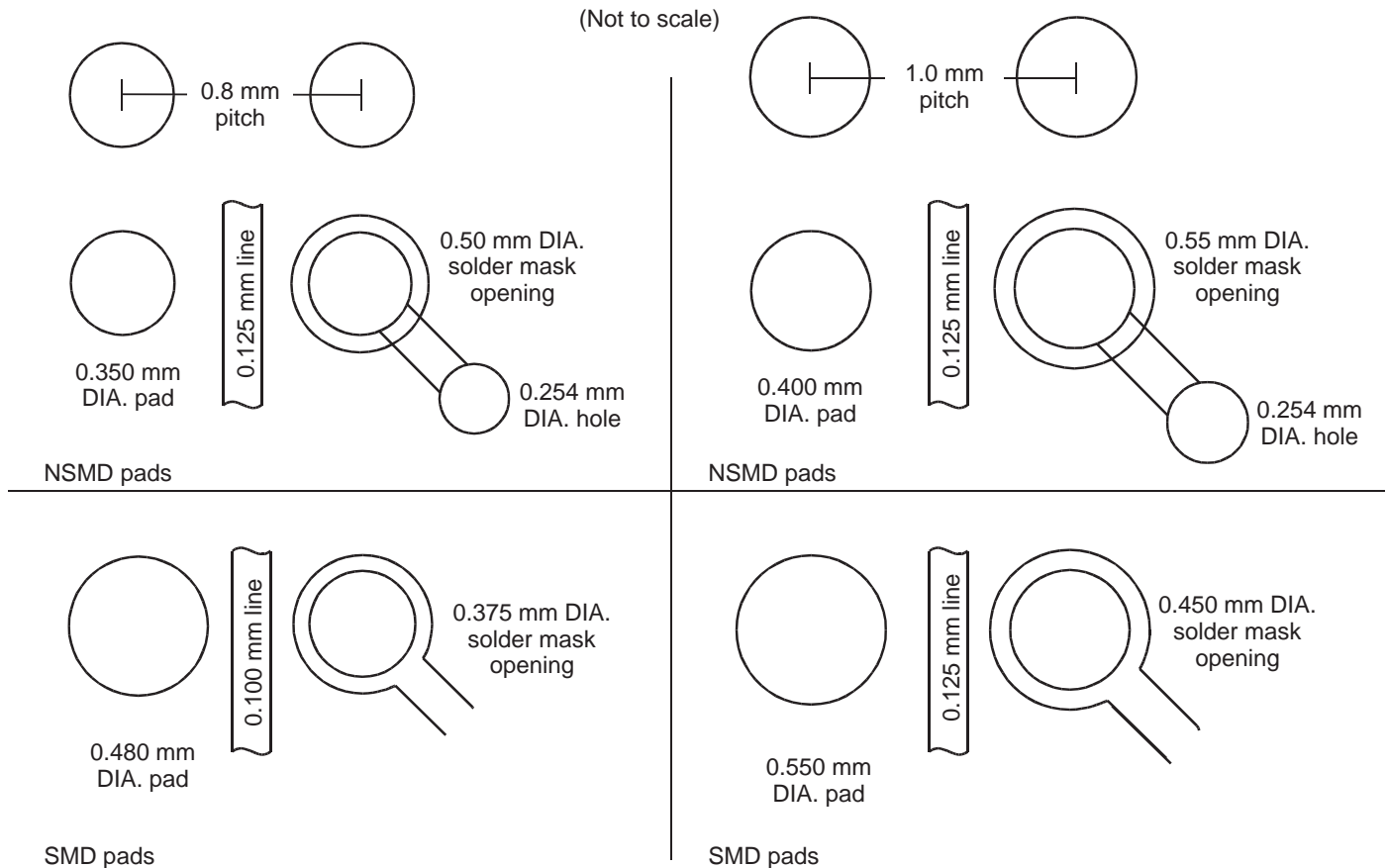
See Figure 8 for an example of optimum land diameters and configurations for a common MicroStar BGA pitch.

Conductor Width/Spacing

Many of today's circuit board layouts are based on at most a 100- μ m conductor line width and 200- μ m spacing. To route between 0.8-mm-pitch balls, given a clearance of roughly 380 μ m between ball lands, only one signal can be routed between ball pads. The 380- μ m ball spacing is worst case and is calculated by assuming the diameter of the solder ball land is 410 μ m.

Figure 9 presents some design considerations based on commonly used PCB design rules. Conventionally, the pads are connected by wide copper traces to other devices or to plated through holes (PTH). As a rule, the mounting pads must be isolated from the PTH. Placing the PTH interstitially to the land pads often achieves this.

Figure 9. PCB Design Considerations (Conventional)



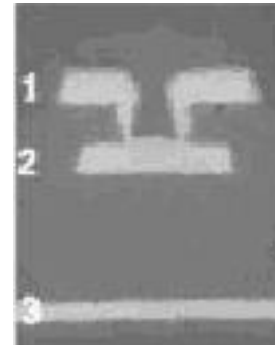
High-Density Routing Techniques

A challenge when designing with CSP packages is that as available space contracts, the space available for signal fanout also decreases. By using a few high-density routing techniques, the PCB designer can minimize many of these design and manufacturing challenges. This section focuses on TI designators GGU (144-pin) and GW (176-pin) packages. Both packages have 0.8-mm pitch, but each is distinctly different in array style. The GGU ball array has wide channels in the four corners, providing the inner balls with space for routing and V_{CC} connectivity. Mechanical drawings of these MicroStar BGA packages can be found in Appendix B. The GGU package has a solid four-row array configuration which can cause difficulties when routing inner rows on two-layer boards.

Via Density

Via density, as mentioned earlier, can be a limiting factor when designing high-density boards. Via density is defined as the number of vias in a particular board area. Using smaller vias increases the routability of the board by requiring less board space and increasing via density. The invention of the microvia, shown in Figure 10, has solved many of the problems associated with via density.

Figure 10. Microvia Structure



Microvias are often created using a laser to penetrate the first few layers of dielectric. The laser can penetrate a 4-mil-thick dielectric layer, creating the 4- μ m microvia shown in Figure 10. The layout designer can now route to the first internal board layer. Two layers (each 4 mils thick) can be laser-drilled, creating a 200- μ m microvia diameter. In this case, routing to the first two internal layers is possible.

The number of board layers increases as board chip density and functional pin count increase. As an example, the TMS320VC549GGU digital signal processor (DSP) is in a 144-GGU package and uses 32 balls for power and ground. Routing of roughly

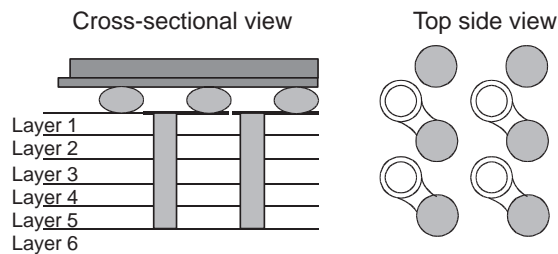
112 signals can be accomplished on three layers. The power and ground planes increase the board to five layers. The sixth layer can be used on the bottom side to place discrete components. Furthermore, by increasing the board layer stack-up to eight layers, high-density applications are possible with only 10 to 15 mils between the chips.

Conventional PCB Design

The relatively large via density on the package periphery, mentioned earlier, is caused by limited options when routing the signal from the ball. To reduce or eliminate the via density problem on the periphery of the package, designers can build the PCB vertically from the BGA pad through the internal layers of the board, as shown in Figure 11. By working vertically and mechanical drilling 250- μ m vias between the pads on the board and the internal layers, designers can create a “pick-and-choose” method. They can pick the layer and choose the route. A “dog bone” method is used to connect the through-hole via and the pad.

This method requires a very small mechanical drill to create the necessary number of 144 or 176 vias for one package. Although this method is the least expensive, a disadvantage is that the vias go through the board, creating a matrix of vias on the bottom side of the board.

Figure 11. “Dog Bone Via” Structure



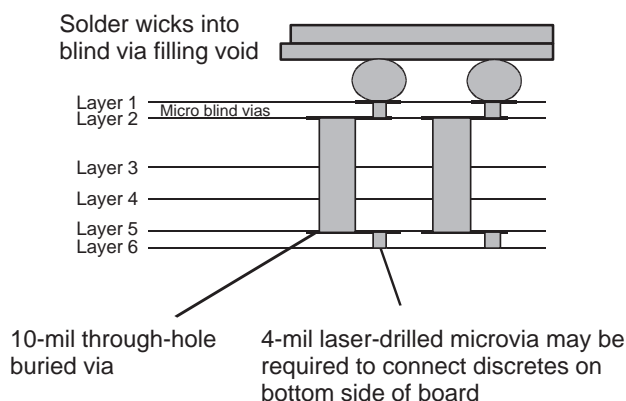
Advanced Design Methods

Another option is to use a combination of blind and buried vias. Blind vias connect either the top or bottom side of the board to inner layers. Buried vias usually connect only the inner layers. Figure 12 illustrates this method using 4-mil laser-drilled microvias in the center of the pads and burying the dog bone on layer 2.

Since the buried via does not extend through the underside of the board, the designer can use another set of laser-drilled blind microvias, if needed, to connect the bypass capacitors and other discrete components to the bottom side.

More information on these advanced techniques is available by contacting your local TI field sales office.

Figure 12. Buried Vias



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Reliability

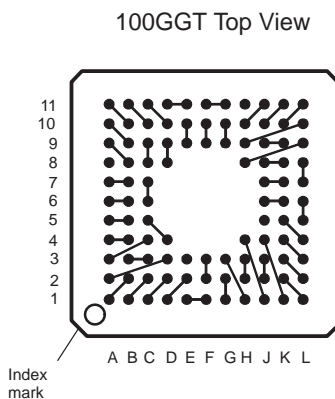
Daisy-Chained Units

Daisy-chained units are used to gain experience in the handling and mounting of CSPs, for board-reliability testing, to check PCB electrical layouts, and to confirm the accuracy of the mounting equipment. To facilitate this, Texas Instruments offers daisy-chained units in all production MicroStar BGA packages.

Each daisy-chained pinout differs slightly depending on package layout. An example is shown in Figure 13. Daisy-chained packages are wired to provide a continuous path through the package for easy testing. TI issues a net list for each package, which correlates each ball position with a corresponding wire pad number. The daisy-chained net list is a special case of the general net list shown in Figure 14. Package net lists and daisy-chained net lists for all production packages are included in Appendix B.

A PCB layout for a 144-GGU daisy-chained package is shown in Figure 15. When a daisy-chained package is assembled on the PCB, a complete circuit is formed, which allows continuity testing. The circuit includes the solder balls, the metal pattern on the die, the bond wires, and the PCB traces. The entire package or only a quadrant can be interconnected and tested. A diagram of the test configuration is shown in Figure 16.

Figure 13. Daisy-Chained Pinout List



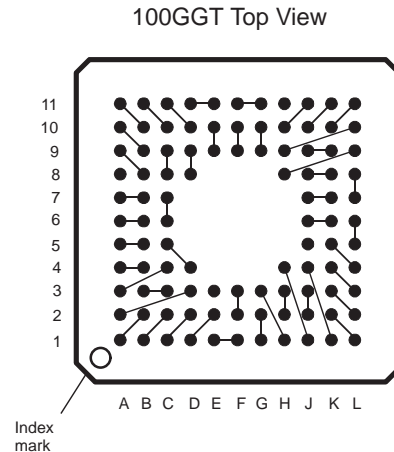
A1 - B2	L1 - K2	L11 - K10	A11 - B10
B1 - C2	L2 - K3	K11 - J10	A10 - B9
C1 - D2	L3 - K4	J11 - H10	A9 - B8
D1 - E2	L4 - K5	G9 - G10	B7 - A7
F3 - F2	J6 - K6	F9 - F10	C7 - C6
E1 - F1	L5 - L6	G11 - F11	B6 - A6
G1 - G2	L7 - L8	E11 - D11	B5 - A5
G3 - H1	K7 - J7	E10 - E9	C5 - D4
H2 - H3	K8 - J8	D10 - C11	A4 - B4
H4 - J1	L9 - H8	D9 - D8	C4 - A3
J2 - J3	K9 - J9	C10 - B11	B3 - C3
K1 - J4	L10 - H9	C9 - C8	A2 - D3

NC - E3, J5, H11, A8

Reliability Data

Reliability is one of the first questions designers ask about any new packaging technology. They want to know how well the package will survive handling and assembly operation, and how long it will last on the board. The elements of package reliability and system reliability, while related, focus on different material properties and characteristics and are tested by different methods.

Figure 14. General Net List



PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1 -	A1	26 -	L1	51 -	L11	76 -	A11
2 -	B2	27 -	K2	52 -	K10	77 -	B10
3 -	B1	28 -	L2	53 -	K11	78 -	A10
4 -	C2	29 -	K3	54 -	J10	79 -	B9
5 -	C1	30 -	L3	55 -	J11	80 -	A9
6 -	D2	31 -	K4	56 -	H10	81 -	B8
7 -	E3	32 -	J5	57 -	H11	82 -	A8
8 -	D1	33 -	L4	58 -	G9	83 -	B7
9 -	E2	34 -	K5	59 -	G10	84 -	A7
10 -	F3	35 -	J6	60 -	F9	85 -	C7
11 -	F2	36 -	K6	61 -	F10	86 -	C6
12 -	E1	37 -	L5	62 -	G11	87 -	B6
13 -	F1	38 -	L6	63 -	F11	88 -	A6
14 -	G1	39 -	L7	64 -	E11	89 -	B5
15 -	G2	40 -	L8	65 -	D11	90 -	A5
16 -	G3	41 -	K7	66 -	E10	91 -	C5
17 -	H1	42 -	J7	67 -	E9	92 -	D4
18 -	H2	43 -	K8	68 -	D10	93 -	A4
19 -	H3	44 -	J8	69 -	C11	94 -	B4
20 -	H4	45 -	L9	70 -	D9	95 -	C4
21 -	J1	46 -	H8	71 -	D8	96 -	A3
22 -	J2	47 -	K9	72 -	C10	97 -	B3
23 -	J3	48 -	J9	73 -	B11	98 -	C3
24 -	K1	49 -	L10	74 -	C9	99 -	A2
25 -	J4	50 -	H9	75 -	C8	100 -	D3

Figure 15. PCB Layout for Daisy-Chained Unit

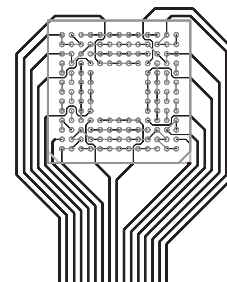
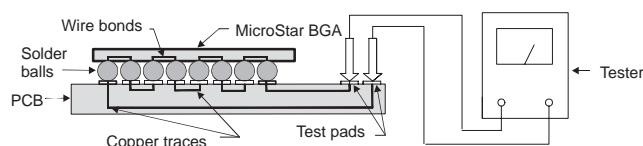


Figure 16. Daisy-Chain Test Configuration

Package reliability focuses on materials of construction, thermal flows, material adherence/delamination issues, resistance to high temperatures, moisture resistance and ball/stitch bond reliability. Thorough engineering of the package is performed to prevent delamination caused by the interaction of the substrate material and the mold compound.

TI subjects each MicroStar BGA to rigorous qualification testing before the package is released to production. These tests are summarized in Table 1. All samples used in these tests are preconditioned according to Joint Electronic Device Committee (JEDEC) A113 at various levels. Typical data is presented in Table 2. MicroStar BGA packages have proven robust and reliable.

Board-level reliability (BLR) issues generally focus on the complex interaction of various materials under the influence of heat generated by the operation of electronic devices. Not only is there a complex thermal situation caused by multiple heat sources, but there are cyclical strains due to expansion mismatches, warping and transient conditions, non-linear material properties, and solder fatigue behavior influenced by geometry, metallurgy, stress relaxation phenomenon, and cycle conditions. In addition to material issues, board and package design can influence reliability. Thermal management from a system level is critical for optimum

reliability, and thermal cycling tests are generally used to predict behavior and reliability. Many of these are used in conjunction with solder fatigue life models using a modified Coffin-Manson strain range-fatigue life plots.

Table 1. Package-Level Reliability Tests†

Test Environments	Conditions	Read Points
HAST	85RH/85°C	600 hrs. 1000 hrs.
Autoclave	121°C, 15 psig	96 hrs. 240 hrs.
Temp. Cycle	-55/125°C -65/150°C‡	500 cycles 750 cycles 1000 cycles
Thermal Shock	-65/150°C‡ -55/125°C	200 cycles 500 cycles 750 cycles 1000 cycles
HTOL	125°C, Op. voltage	500 hrs. 600 hrs. 1000 hrs.
HTOL‡	140°C, Op. voltage	500 hrs.
HTOL‡	155°C, Op. voltage	240 hrs.
Bake‡	150°C	600 hrs. 1000 hrs.
	170°C	420 hrs.
HAST‡	130°C	96 hrs.

† All samples used in these tests are preconditioned according to Joint Electronic Device Committee (JEDEC) A113 at various levels.

‡ Optional tests. One or more of them may be added to meet customer requirements.

Table 2. Package-Level Reliability Test Results

Package Types							
	Leads	64	80	144		196	
	Body (mm)	8 x 8	10 x 10	12 x 12		15 x 15	
	Device	MSP	ASP	DSP		DSP	
	Die (mm)	5.3 x 5.8	7.5 x 7.5	9.3 x 9.5			
	Level	4	2	2a	4	3	
Test Environment		Failures/Sample Size					
Autoclave	(240 hrs.)	0/70	0/78	0/77	0/77	0/77	
T/C, −55/125°C	(1000 cycles)	0/116	0/78	0/77	0/77	0/76	
T/S, −65/150°C	(500 cycles)		0/78	0/77	0/77	0/77	
	(750 cycles)						
	(1000 cycles)	0/116			0/77	0/77	
HAST, 85°C/85%RH	(1000 hrs.) (1250 hrs.)	0/115		0/77		0/78	
150°C Storage	(600 hrs.) (1000 hrs.)	0/43	0/78		0/77	0/77	0/77
HTOL	(1000 hrs.)	0/116					

In addition to device/package testing, board-level reliability testing has been extensively performed on the MicroStar BGA packages. Various types of daisy-chained packages were assembled to special boards shown in Figure 17. Electrical measurements

Figure 17. Board-Level Reliability Test Boards

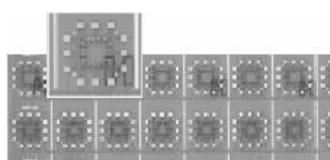
Board Material FR-4

Structure: Two external metal layers
Traces: 1oz cu design rule
 100 μm (4 mils) width,
 100 μm (4 mils) space
Paste: Eutectic (SENJU 63-330F-21-10.5)
Paste thickness: 0.15 μm
Board thickness: 31 mils

Reflow profile: 225°C max, time above 200°C is 50 sec, time above 150°C is 240 sec
Screen opening: match land pad diameter
Precondition: Level 3



TI-Houston test board



TI-HIJI test board

were made in the initial state and then at intervals after temperature cycles were run. The overall test conditions are shown in Figure 18. A summary of a wide range of board-level reliability is shown in Table 3. This data includes testing by TI and by end manufacturers.

Table 4 summarizes conclusions from the testing. Two important conclusions are that the PCB pad size needs to match the via size, and that solder paste is needed for attachment to give optimal reliability.

Reliability Calculations

Another important aspect of predicting how a package will perform in any given application is reliability modeling. Thermal, electrical, and thermomechanical modeling, verified by experimental results, provide insight into system behavior, shorten package

Figure 18. Board-Level Reliability Test Data

Test condition: Open short @25°C, 10% resistance change or 200 Ω

Sample size: Greater or equal to 32

Temperature cycle range: -40°C to 125°C

Sampling rate: Every 100 cycles, up to first failure; every 50 cycles thereafter up to 1000 cycles; every 100 cycles between 1000 to 1500 cycles; every 250 cycles between 1500 to 2500 cycles; Test stopping point min (2500 cycles, 50% failures)

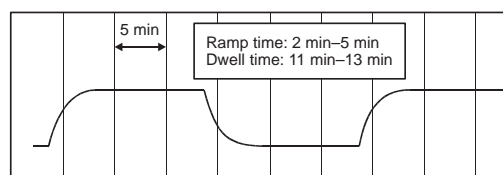


Table 3. Board-Level Reliability Summary

Conditions (With Solder Paste)						Failures/Sample Size						
						Requirements			Extended Range			
						500	800	1000	1100	1200	1300	1500
Package	TI Mfg Site Test Site	Body (mm)	Pitch (mm)	Die (mm)	Temp. Cycle (°C)	(Cycles)			(Cycles)			
GGU 144 balls	TI HIJI TI HIJI	12 x 12	0.8	8.8 x 8.8	-40/125	0/85	0/85	0/85	4/85	5/77	5/72	15/39
GGU 144 balls	TI Philippines TI HIJI	12 x 12	0.8	8.8 x 8.8	-40/125	0/36	0/36	0/36	0/36	0/36	0/36	1/35
GGF 100 balls	TI HIJI TI HIJI	10 x 10	0.5	6.6 x 6.6	-25/125	0/32	0/32	0/32	0/32	0/32	0/16	6/16
GHC 196 balls	TI TIPI TI Hou	15 x 15	1.0	8.8 x 8.8	-40/125	0/62	0/62	0/62	0/62	0/62	0/62	4/62
GGU 144 balls	TI Philippines Customer A	12 x 12	0.8	8.8 x 8.8	-40/100	0/180	0/180	0/180	0/180	—	—	—
GGW 176 balls	TI HIJI Customer B	15 x 15	0.8	6.6 x 6.6	-25/125	0/35	0/35	0/35	0/35	0/35	0/35	1/35
GGM 80 balls	TI HIJI Customer C	10 x 10	0.8	5.0 x 5.0	-40/125	0/12	0/12	0/12	—	—	—	0/10

Table 4. Summary of Significant BLR Improvements

Condition		Improved BLR ⇒
Die size	Larger	⇒ Smaller
Die edge	Over balls	⇒ Within ball matrix
Ball count	Smaller	⇒ Larger
Ball size	Smaller	⇒ Larger
PCB pad size	Over/undersized	⇒ Matches package via (for NSMD ~90% of via)
Solder paste	None or insufficient	⇒ Thickness 0.15 nom. (type matches reflow)

development time, predict system lifetimes, and provide an important analytical tool. In applications such as BGAs, where the interconnections are made through solder balls, the useful life of the package is, in most cases, dependent on the useful life of the solder itself. This is an area that has been studied extensively, and very accurate models for predicting both solder behavior and interpreting accelerated life testing exist.

The current methodology employed at Texas Instruments includes both extensive model refinement and constant experimental verification. For a given package, a detailed 2D Finite Element Model (FEM) is constructed. This model will be used to carry out 2D plain strain elastoplastic analysis to predict areas of high stress. These models also account for the thermal variation of material properties, such as Modulus of Elasticity, Coefficient of Thermal Expansion, and Poisson's Ratio as a function of temperature. These allow the FEM to calculate the thermomechanical plastic strains in the solder joints for a given thermal loading.

The combination of Finite Element Analysis (FEA), accurate thermal property information, and advanced statistical methods allows prediction of the number of cycles to failure for various probability levels. Using the assumption that cyclic fatigue lifetime follows a Weibull distribution, various probability levels can be calculated. For these calculations, the Weibull shape parameter used is $\beta = 4$, which is based on experimental data calibration. It is also consistent with available experimental data found in the literature for leadless packages. This then results in the following equation:

$$Nf(x\%) = Nf(50\%) [\ln(1-0.01x)/\ln(0.5)]^{1/\beta}$$

Using this equation, and using the plastic strain ϵ_p in combination with the S-N curves, the data below is an example of the accuracy possible with this method:

Sample Finite Element Simulation and Life Prediction:

144 GGU @ T/C: -40/125°C

{Model} → $\epsilon_p = 0.353\%$ on the outmost joint
→ $Nf(50\%) = 4434$ cycles

→ $Nf(1\%) = 1539$ cycles

{BLR Testing} → -40/125°C (10 min/10 min)
→ $Nf(1\%) = 1657$ cycles

Modeling is most useful in exploring changes in materials, designs and process parameters without the need to build experimental units. For example, modeling was used to study the effects of changes in board thickness and pad size. Table 5 shows the simulated effects of pad size and board thickness on the fatigue life of a 144-GGU package.

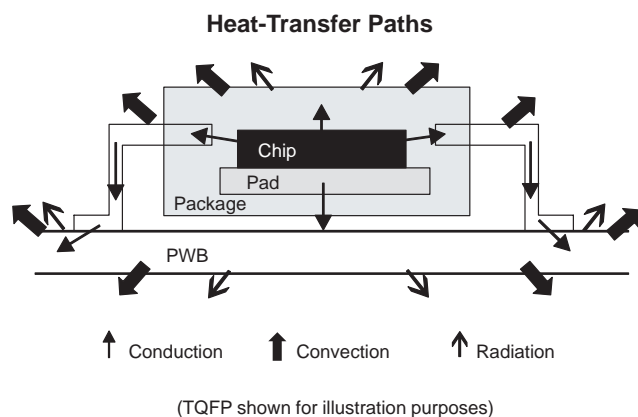
Table 5. Effects of Pad Size and Board Thickness on Fatigue Life

Example1: Effects of pad size on fatigue life <ul style="list-style-type: none">● Package: 144 GGU● Die: 8.8 x 8.8 x 0.279 mm● Board: FR-4 board 52 mils thick	Pad Dia. (mils)	Pad Standoff (mm)	Solder Center Dia. (mm)	Plastic Strain (%)	Nf (1%) (cycles to failure)	Difference
	12	0.3847	0.4908	0.4400	998	0.88x
	13	0.3689	0.4951	0.4127	1134	1
	14	0.3523	0.5005	0.3908	1263	1.11x
	15	0.3350	0.5060	0.3741	1377	1.21x
Example 2: Effects of board thickness on fatigue life <ul style="list-style-type: none">● Package: 144 GGU● Die: 8.8 x 8.8 x 0.279 mm● Board: FR-4● Pad Size: 13 mils	Board Thickness (mils)	Plastic Strain (%)	Nf (1%) (cycles to failure)	Difference		
	50	0.4095	1152	1		
	31	0.393	1249	1.08x		

Package Characteristics

Texas Instruments has extensive package characterization capabilities, including an electrical measurements lab with TDR/LRC (Time Domain Reflectometer/inductance resistance capacitance) and network analysis capabilities, a thermal measurements lab with JEDEC standard test conditions up to 1000 watts, and extensive electrical, thermal, and mechanical modeling capability. Modeling was implemented at TI starting in 1984. Stress analysis is done with the Ansys Analysis tool, which provides full linear, nonlinear, 2D and 3D capabilities for solder reliability, package warpage, and stress analysis studies. An internally developed tool (PACED™) is used for electrical modeling that gives 2.5D and full 3D capability for LRC models, transmission lines, lossy dielectrics, and SPICE deck outputs. The thermal modeling tool was also internally developed (ThermCAL™) and it provides full 3D automatic mesh generation for most packages.

Figure 19. Thermal Modeling Process



- **Model's three heat-transfer mechanisms:**
 - Conduction
 - Convection
 - Radiation
- **Method:**
 - Define solid
 - Mesh solid
 - Solve large number of simultaneous equations relating each defined mesh point to each other
- **Sources of error:**
 - Convection coefficients
 - Material properties
 - Solid definition inaccuracies

Complex geometries, transient analysis, and anisotropic materials can be modeled with it. With these capabilities, a full range of modeling from device level through system level can be provided. Package modeling is used to predict package performance at the design stage, to provide a package development tool, to aid qualification by similarity, and is used as a failure analysis tool.

Thermal Modeling

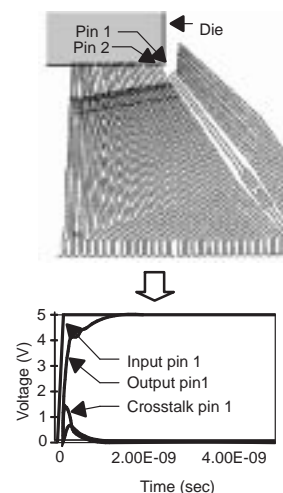
Figure 19 outlines the thermal modeling process. Data for each package is included in Appendix B.

Electrical Modeling

Figure 20 outlines the electrical modeling process. Data for each package is included in Appendix B.

Figure 20. Electrical Modeling Process

- Calculates inductances, capacitances, resistances, transmission line characteristics of package geometries
- Uses as loads for circuit simulation
- Process
 - Select solution algorithms for problem domain
 - Identify package structures to be modeled
 - Generate spice deck of package parameters
 - Simulate impact on driver output waveforms
 - Calculate ground/power bounce



3

Surface-Mounting MicroStar BGA Packages

Surface-mount technology (SMT) has evolved over the past decade from an art into a science with the development of design guidelines and rules. While these guidelines are specific enough to incorporate many shared conclusions, they are general enough to allow flexibility in board layouts, solder pastes, stencils, fixturing, and reflow profiles. From experience, most assembly operations have found MicroStar BGA packages to be robust, manufacturing-friendly packages that fit easily within existing processes and profiles. In addition, they do not require special handling. However, as ball pitch becomes smaller, layout methodology and placement accuracy become more critical. Below is a review of the more important aspects of surface-mounted CSPs. The suggestions provided may aid in efficient, cost-effective production.

Design for Manufacturability (DFM)

A well-designed board that follows the basic surface-mount technology considerations greatly improves the cost, cycle time, and quality of the end product. Board design should comprehend the SMT-automated equipment used for assembly, including minimum and maximum dimensional limits and placement accuracy. Many board shapes can be accommodated, but the front of the board should have a straight and square edge to help machine sensors detect it. While odd-shaped or small boards can be assembled, they require panelization or special tooling to process in-line. The more irregular the board—non-rectangular with no cutouts—the more expensive the assembly cost.

Fiducials (the optical alignment targets that align the module to the automated equipment) should allow vision-assisted equipment to accommodate the shrink and stretch of the raw board during processing. They also define the coordinate system for all automated equipment, such as printing and pick-and-place. The following guidelines may be helpful:

- Automated equipment requires a minimum of two and preferably three fiducials.
- A wide range of fiducial shapes and sizes can be used. Among the most useful is a circle 1.6 mm in diameter with an annulus of 3.175/3.71 mm. The outer ring is optional, but no other feature may be within 0.76 mm of the fiducial.
- The most useful placement for the fiducials is an L configuration, which is orthogonal to optimize the stretch/shrink algorithms. When possible, the lower left fiducial should be the design origin (coordinate 0,0).
- All components should be within 101.6 mm of a fiducial to guarantee placement accuracy. For large boards or panels, a fourth fiducial should be added.

If the edges of the boards are to be used for conveyer transfer, a cleared zone of at least 3.17 mm should be allowed. Normally, the longest edges of the board are used for this purpose, and the actual width is dependent on equipment capability. While no component lands or fiducials can be in this area, breakaway tabs may be.

Interpackage spacing is a key aspect of DFM, and the question of how close you can safely put components to each other is a critical one. The following component layout considerations are recommendations based on TI experience:

- There should be a minimum of 0.508 mm between land areas of adjacent components to reduce the risk of shorting.
- The recommended minimum spacing between SMD discrete component bodies is equal to the height of the tallest component. This allows for a 45° soldering angle in case manual work is needed.
- Polarization symbols need to be provided for discrete SMDs (diodes, capacitors, etc.) next to the positive pin.
- Pin-1 indicators or features are needed to determine the keying of SMD components.
- Space between lands (under components) on the backside discrete components should be a minimum of 0.33 mm. No open vias may be in this space.
- The direction of backside discretes for wave solder should be perpendicular to the direction through the wave.
- Do not put SMT components on the bottom side that exceed 200 grams per square inch of contact area with the board.
- If space permits, symbolize all reference designators within the land pattern of the respective components.
- It is preferable to have all components oriented in well-ordered columns and rows.
- Group similar components together whenever possible.
- Room for testing needs to be allowed.

Solder Paste

TI recommends the use of paste when mounting MicroStar BGAs. The use of paste offers the following advantages:

- It acts as a flux to aid wetting of the solder ball to the PCB land.
- The adhesive properties of the paste will hold the component in place during reflow.

- It helps compensate for minor variations in the planarity of the solder balls.
- Paste contributes to the final volume of solder in the joint, and thus allows this volume to be varied to give an optimum joint.

Paste selection is normally driven by overall system assembly requirements. In general, the “no clean” compositions are preferred due to the difficulty in cleaning under the mounted component. Most assembly operations have found that no changes in existing pastes are required by the addition of MicroStar BGA, but due to the large variety of board designs and tolerances, it is not possible to say this will be true for any specific application.

Nearly as critical as paste selection is stencil design. A proactive approach to stencil design can pay large dividends in assembly yields and lower costs. In general, MicroStar BGA packages are special cases of BGA packages, and the general design guidelines for BGA package assembly applies to them as well. There are some excellent papers on BGA assembly, so only a brief overview of issues especially important to MicroStar BGA packages will be presented here.

The typical stencil hole diameter should be the same size as the land area, and 125- to 150- μm -thick stencils have been found to give the best results. Good release and a consistent amount of solder paste and shapes are critical, especially as ball pitches decrease. The use of metal squeegee blades, or at the very least, high durometer polyblades, is important in achieving this. Paste viscosity and consistency during screening are some variables that require close control.

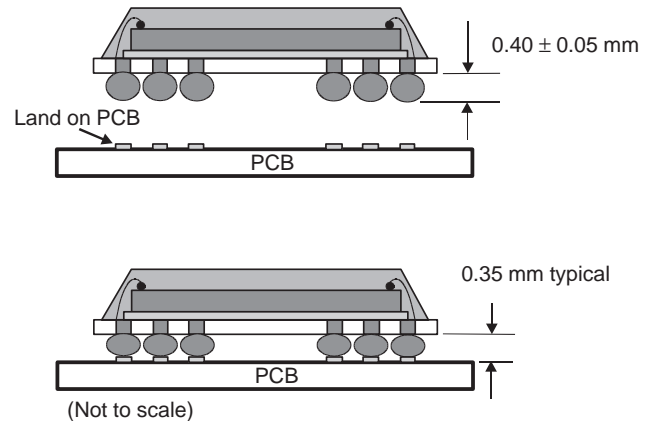
Solder Ball Collapse

In order to produce the optimum solder joint, it is important to understand the amount of collapse of the solder balls, and the overall shape of the joint. These are a function of:

- The diameter of the package solder ball via.
- The volume and type of paste screened onto the PCB.
- The diameter of the PCB land.
- The board assembly reflow conditions.
- The weight of the package.

The original ball height on the package for a typical 0.8-mm-pitch package is 0.40 mm. After the package is mounted, this typically drops to 0.35 mm, as illustrated in Figure 21.

Figure 21. Solder Ball Collapse



Controlling the collapse, and thus defining the package standoff, is critical to obtaining the optimum joint reliability. Generally, a larger standoff gives better solder joint fatigue strength, but this should not be achieved by reducing the board land diameter. Reducing the land diameter will increase the standoff, but will also reduce the minimum cross-section area of the joint. This, in turn, will increase the maximum shear force at the PCB side of the solder joint. Thus, a reduction of land diameter will normally result in a worse fatigue life, and should be avoided unless all the consequences are well understood.

Reflow

Solder reflow conditions are the next critical step in the mounting process. During reflow, the solvent in the solder paste evaporates, the flux cleans the metal surfaces, the solder particles melt, wetting of the surfaces takes place by wicking of molten solder, the solder balls collapse, and finally solidification of the solder into a strong metallurgical bond completes the process. The desired end result is a uniform solder structure strongly bonded to both the PCB and the package with small or no voids and a smooth, even fillet at both ends. Conversely, when all the steps do not carefully fit together, voids, gaps, uneven joint thickness, discontinuities, and insufficient fillet can occur. While the exact cycle used depends on the reflow system and paste composition, there are several key points all successful cycles have in common.

The first of these is a warm-up period sufficient to safely evaporate the solvent. This can be done with a pre-heat or a bake, or, more commonly, a hold in the cycle at evaporation temperatures. If there is less solvent in the paste (such as in a high-viscosity, high-metal-content paste), then the hold can be shorter. However, when the hold is not long enough to get all of the solvent out or too fast to allow it to evaporate, many negative things happen. These range from solder-particle splatter to

trapped gases, which can cause voids and embrittlement. A significant number of reliability problems with solder joints can be solved with the warm-up step, so it needs careful attention.

The second key point that successful reflow cycles have in common is uniform heating across the package and the board. Uneven solder thickness and non-uniform solder joints may be an indicator that the profile needs adjustment. There can also be a problem when different sized components are reflowed at the same time. Care needs to be taken when profiling an oven to be sure that the indicated temperatures are representative of what the most difficult to reflow parts are seeing. These problems are more pronounced with some reflow methods, such as infrared (IR) reflow, than with others, such as forced hot-air convection.

Finally, successful reflow cycles strike a balance among temperature, timing, and length of cycle. Mistiming may lead to excessive fluxing activation, oxidation, excessive voiding, or even damage to the package. Heating the paste too hot too fast before it melts can also dry the paste, which leads to poor wetting. Process development is needed to optimize reflow profiles for each solder paste/flux combination.

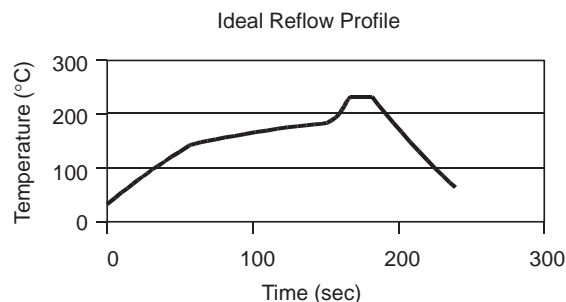
The profile shown in Figure 22 is an ideal one for use in a forced-air-convection furnace, which is the most highly recommended type. The best results have been found in a nitrogen atmosphere.

The guidelines upon which this profile is based, also shown in Figure 22, are general. Modification to the ideal reflow profile will be driven by the interplay of solder-paste particle size and flux percentage with process variables such as heating rates, peak temperatures, board construction factors and atmosphere. These modifications are dependent upon specific applications.

It should be noted that while they are more rugged than most CSP-type packages, many MicroStar BGA packages are still slightly moisture-sensitive at the time of printing of this Reference Guide. The time out of a dry environment should be controlled according to the label on the packing material. This will prevent moisture absorption problems with the package such as “popcorning,” or delamination.

Figure 22. Ideal Reflow Profile

RT to 140°C:	60–90 sec
140°C to 180°C:	60–120 sec
Time above 183°C:	60–150 sec
Peak temperature:	220°C ± 5°C
Time within 5°C peak temperature:	10–20 sec
Ramp-down rate:	6°C/sec maximum



Note: This is an ideal profile, and actual conditions obtained in any specific reflow oven will vary. This profile is based on convection or RF plus forced convection heating.

Other concerns with BGA packages are those caused by a PCB bowing or twisting during reflow. As PCBs get thinner, these problems will become more significant. Potential problems from these effects will show up as open pins, hourglass solder joints, or solder discontinuities. Proper support of the PCB through the furnace, balancing the tab attachments to a panel, and, in worst cases, using a weight to stiffen the PCB can help prevent this. In general, the small size of CSPs create fewer problems than standard BGAs. It is also true that BGAs generally have fewer problems than leaded components.

Inspection

MicroStar BGA packages have been designed to be consistent with very high-yield assembly processes. Because of their relatively light weight, MicroStar BGA packages tend to self-align during reflow. Since the pitch of the ball pattern is large compared to that of fine-pitch leaded packages, solder bridging is rarely encountered. It is recommended that a high-quality solder joint assembly process be developed using the various inspection and analytical techniques, such as cross-sectioning. Once a quality process has been developed, detailed inspection should not be necessary. Visual methods, while obviously limited, can offer valuable clues to the general stability of the process. Electrical checks can confirm interconnection. Both transmission X-rays and laminographic X-rays have proven to be useful nondestructive tools, if desired.

4

Packing and Shipping

MicroStar BGAs are shipped in either of two packing methods:

- Trays
- Tape and reel

Trays

Thermally resistant plastic trays are currently used to ship the majority of the packages. Each family of parts

with the same package outline has its own individually designed tray. The trays are designed to be used with pick-and-place machines. Figure 23 gives typical tray details, and Table 6 shows the number of units per tray.

Figure 24 shows the packing method used to ship trays. Before the trays are sealed in the aluminum-lined plastic bag, they are baked in accordance with the requirements for dry-packing at the appropriate level.

Figure 23. Shipping Tray Detail

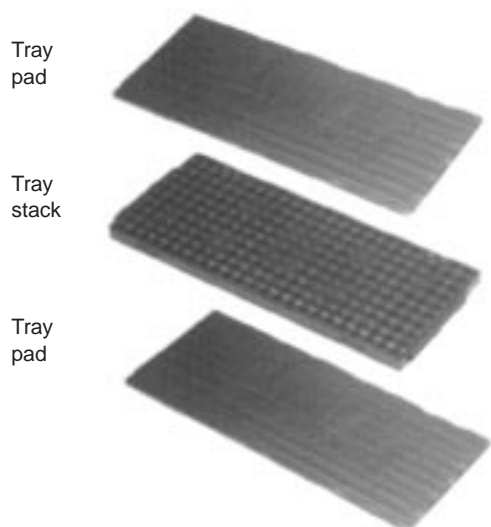


Table 6. Number of Units per Shipping Tray

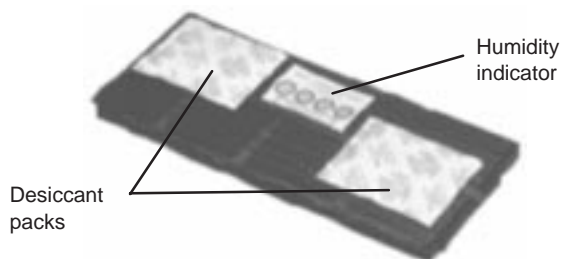
Body Size (mm)	Package Code	Matrix	Units/ Tray	Units/ Box
16 x 16	GZY, GHK	6 x 15	90	450
15 x 15	GGW,GHC	6 x 15	90	450
13 x 13	GHG, GHJ, GHV	8 x 20	160	800
12 x 12	GZG, GGB	8 x 20	160	800
11 x 11	GGT	8 x 20	160	800
10 x 10	GGF, GHZ, GGM	8 x 25	200	1000
8 x 8	GGV, GJJ	9 x 25	225	1125
9 x 13	GFZ, GHB, GHN	10 x 18	180	900

Figure 24. Packing Method for Trays

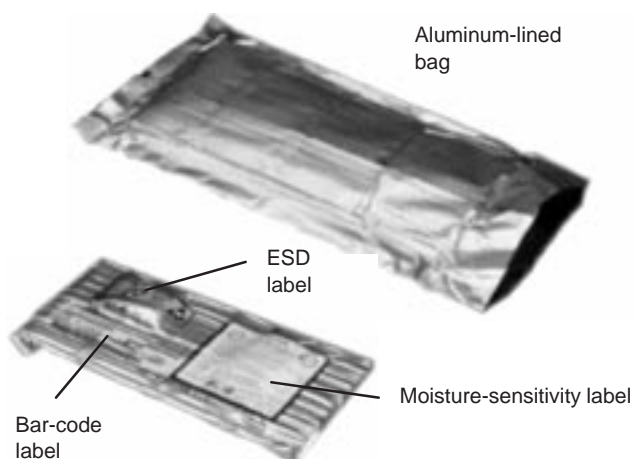
1. Arrange the stack of trays to be packed with a tray pad on top and bottom.



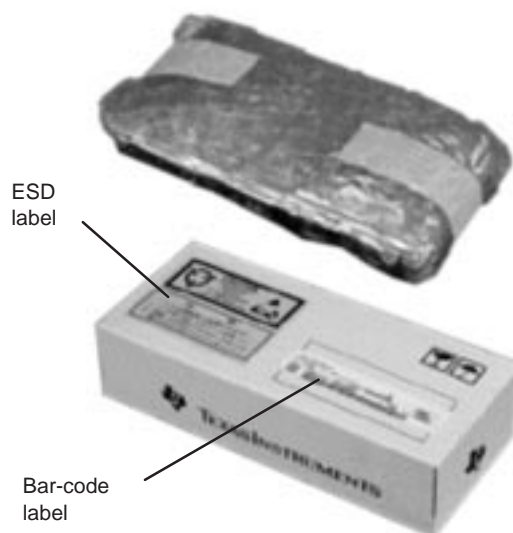
2. Strap the tray stack and pads together with four straps—three crosswise and one lengthwise. Then place the desiccants and the humidity indicator on top.



3. Place the lot inside the aluminum-lined bag and vacuum-seal it. Place the necessary labels on the sealed bag.



4. Wrap and tape bubble pack around the bag for a snug fit in the inner carton. Place the necessary labels on the inner carton.



5. Add bubble pack around the inner carton for a snug fit in the skidboard liner.



6. Place four foam corner spacers on the folded skidboard liner before placing it in the outer carton. An enhanced skidboard liner, which eliminates the need for foam corner spacers, may be used. Seal outer carton and apply necessary labels.



Tape-and-Reel Packing Method

The embossed tape-and-reel method is generally preferred by automatic pick-and-place machines. This will be the standard way MicroStar BGA packages will be shipped. Trays will remain an option for those customers who prefer them. The tape is made from an antistatic/conductive material. The cover tape, which peels back during use, is heat-sealed to the carrier tape to keep the devices in their cavities during shipping and handling. The tape-and-reel packaging used by Texas Instruments is in full compliance with EIA Standard 481-A, "Taping of Surface-Mount Components for Automatic Placement." The static-inhibiting materials used in the carrier-tape manufacturing provides device

protection from static damage, while the rigid, dust-free polystyrene reels provide mechanical protection and clean-room compatibility with dereeling equipment currently available on most high-speed automated placement systems.

Tape Format

Typical tape format is shown in Figure 25. The variables used in Figure 25 and Table 7 are defined as follows: W is the tape width; P is the pocket pitch; A_0 is the pocket width; B_0 is the pocket length; K_0 is the pocket depth; K is the maximum tape depth; and F is the distance between the drive hole and the centerline of the pocket.

Figure 25. Single Sprocket Tape Dimensions

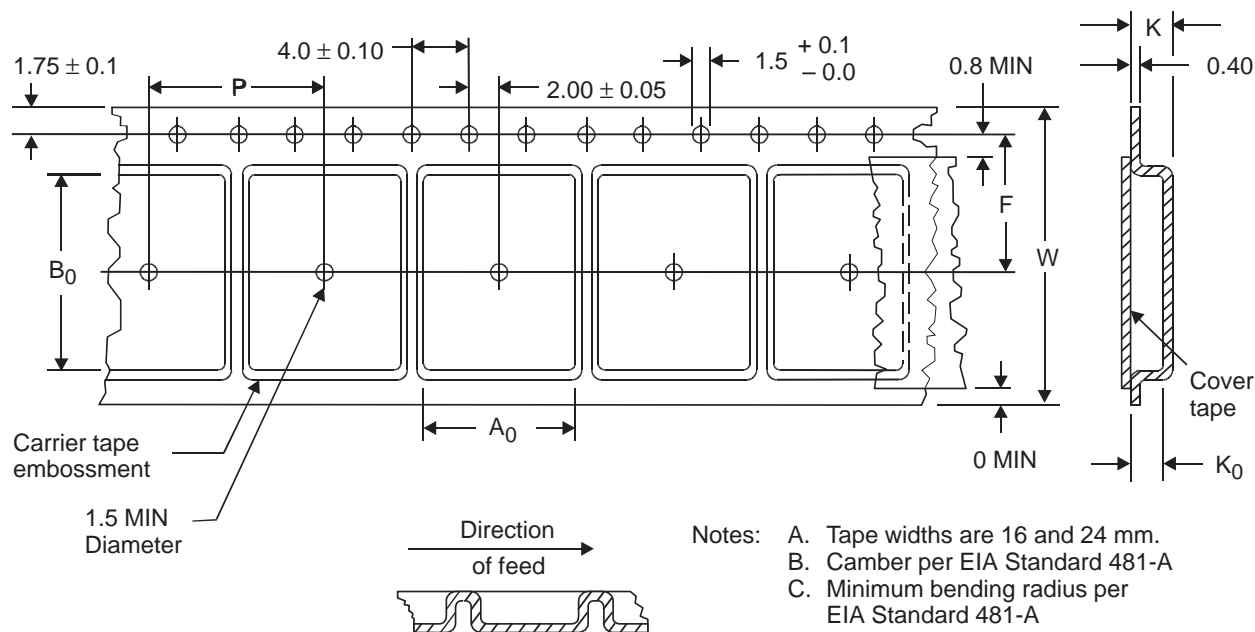
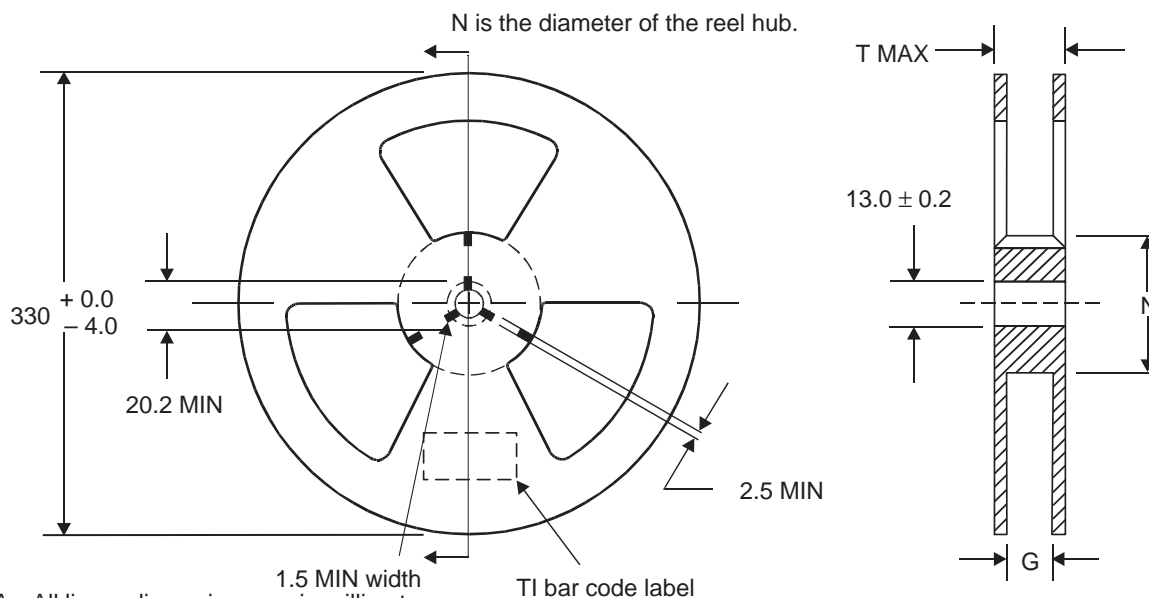


Table 7. Tape Dimensions†

Tape Width (W)	Pocket Pitch (P)	Pocket Width (A_0)	Pocket Length (B_0)	Pocket Depth (K_0)	Max. Tape Depth (K)	Centerline to Drive Hole (F)	Package Size
16	12	8.2	8.2	1.7	2.0	7.5	8 x 8
24	16	10.2	10.2	1.7	2.0	11.5	10 x 10
24	16	11.35	11.35	1.9	2.2	11.5	11 x 11
24	16	12.4	12.4	1.9	2.2	11.5	12 x 12
24	20	15.25	15.25	2.2	2.5	11.5	15 x 15

† All dimensions are in millimeters.

Figure 26. Reel Dimensions

Note A: All linear dimensions are in millimeters.

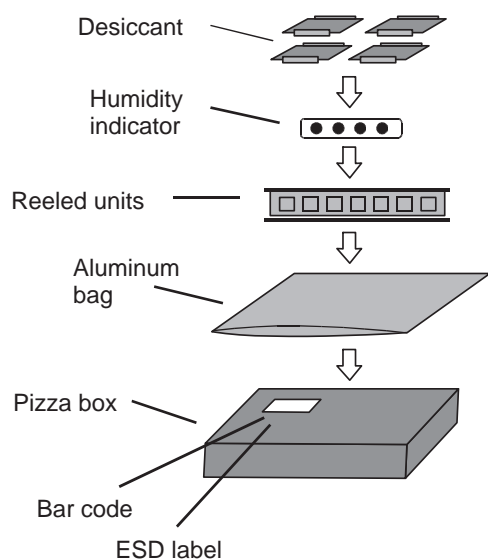
Table 8. Reel Dimensions†

Tape Width (G)	Reel Hub Diameter (N)	Reel Total Thickness (T MAX)	Parts per Reel
16	100	28	1000
24	100	28	1000

† All dimensions are in millimeters.

The reels are shown in Figure 26. In this figure, G is the width of the tape, N is the diameter of the hub, and T is the total reel thickness.

After the parts are loaded into the reel, each individual reel is packed in its own “pizza” box for shipping, as shown in Figure 27.

Figure 27. Tape-and-Reel Packing

Device Insertion

Devices are inserted toward the outer periphery of the tape by placing the side with the device name face up and the side with the balls attached face down. The pin-1 indicator is placed in the top right-hand corner of the pocket, next to the sprocket holes.

Packaging Method

For reels, once the taping has been completed, the end of the leader is fixed onto the reel with tape. The product name, lot number, quantity, and date code are recorded on the reel and the cardboard box used for tape delivery. Each reel is separately packed in a cardboard box for delivery.

Trays are packed with five loaded trays and one empty tray on top for support and to keep packages secure. The stack is secured with stable plastic straps and sealed in a moisture-proof bag.

Customer-specific bar code labels can be added under request or general purchasing specification.

Moisture-sensitive packages are baked before packing and are packed within 8 hours of coming out of the oven. Both the tape-and-reel and the tray moisture-proof bags are sealed and marked with appropriate labeling warning that the packages inside the bags are dry-packed and giving the level of moisture sensitivity.

5

Sockets

The Design Challenge

The fine pitch of MicroStar BGA packages makes socketting a special challenge. Mechanical, thermal, and electrical issues must be accommodated by the socket designer. CSP packaging is at the cutting edge of package design and it appears that it is being adopted faster than any other previous package technology. Standards are only now beginning to be established. TI fully supports these efforts, and all MicroStar BGA outlines are being engineered to fit within JEDEC standards where they exist. For instance, all 0.8-mm-pitch packages fit within JEDEC MO205. While these standards detail the pitch and I/O placement, they do allow wide latitude for overall body size variation. The size of a specific package within the TI MicroStar BGA family is based on the package construction, and is independent of die size. Thus, a range of die sizes and I/Os within a family will have the same package dimensions. Each different family has a specific I/O pitch and array. For maximum socket versatility, an adapter or “personalizer” can be customized for each application, allowing a single-socket body to be used with many packages. This feature is especially useful in the early days as the technology is being developed and adopted and the total volume required is small.

Contacting the Ball

A number of different approaches for contacting the solder ball are shown schematically in Figure 28. The pinch style contact has been used extensively for contacting solder balls in conventional BGAs. A benefit of the pinch style is that the socket does not have to push down on the package to provide the necessary contact force to penetrate the oxide film on the solder balls. The issues in utilizing this approach for pitches below 1.27 mm involve:

1. Miniaturizing the contact
2. Developing injection-molding tooling for the pitch
3. Developing cost-effective manufacturing procedures for handling and assembling the fragile contact

For pitches of 0.75 mm and above, Texas Instruments has designed a pinch contact that satisfies all of these requirements. Further information on the availability of these sockets can be obtained from your local TI Field Sales representative.

The contact is designed to grip the solder ball with a pinching action. This not only provides electrical contact to the solder ball but also helps retain the package in the socket. The contact is shown in Figure 29. The contact is stamped and formed from a 0.12-mm-thick strip of CDA 172, the high-yield-strength beryllium copper alloy. This alloy is used for spring applications that are exposed to high stresses and temperatures because of its excellent stress relaxation performance and formability.

Figure 28. Approaches for Contacting the Solder Ball

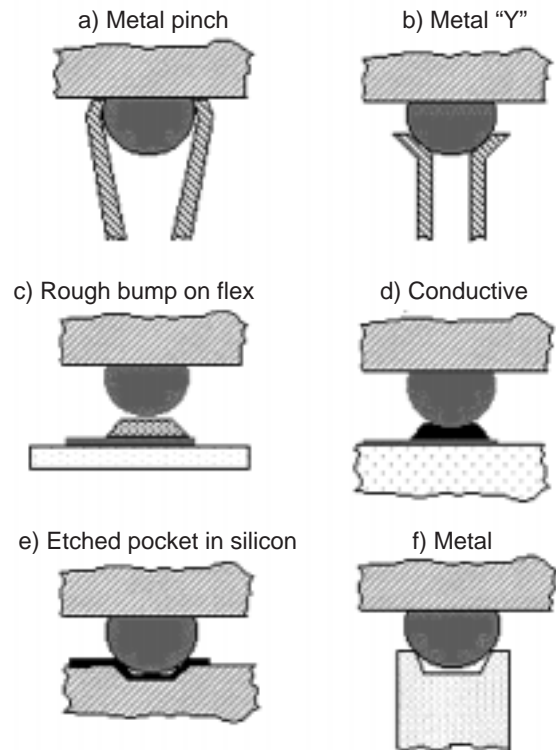
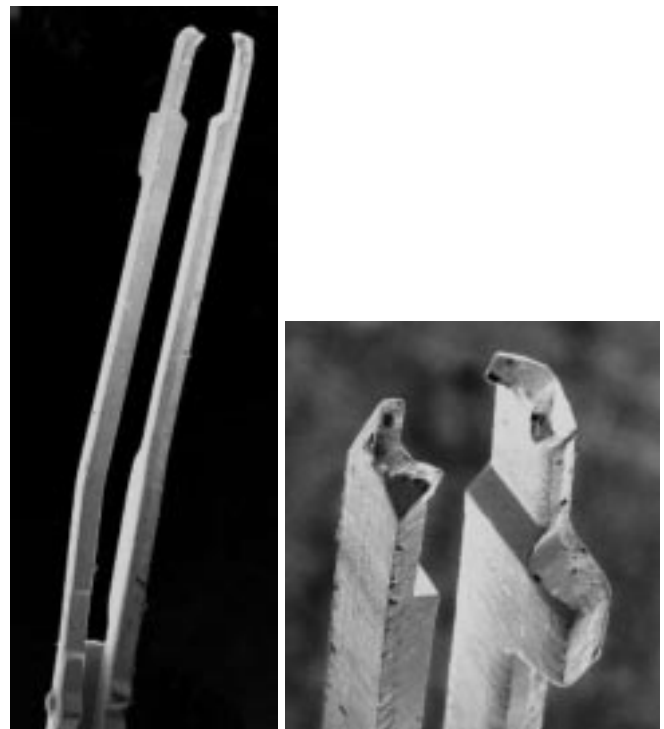


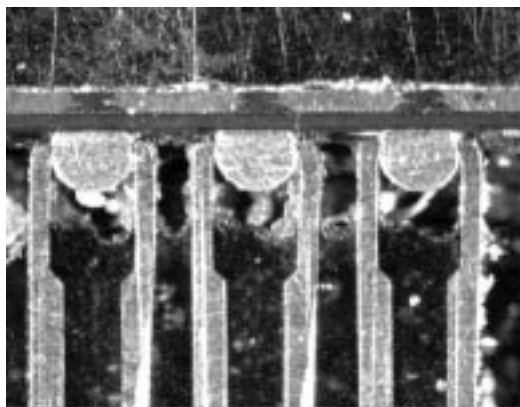
Figure 29. Pinch Contact for Solder Balls



Each contact incorporates two beams that provide an oxide-piercing interface with the sides of the balls above the central area—the equator. Since the contact is above the equator, the resultant force is downward and ensures package retention in the socket. No contact is made on

the bottom of the solder ball and the original package planarity specifications are unchanged. A photomicrograph of the contact touching the solder balls is shown in Figure 30.

Figure 30. Contact Area on Solder Ball



The witness marks left on the solder ball from the contact are shown in Figure 31. This ball was contacted at room temperature and it is clear that there was no damage to the bottom of the ball or any witness marks from the contact above the equator.

The effect of burn-in on the probe marks was examined by simulating a cycle and placing a loaded socket into an oven at 125°C for 9 hours. The result is shown in Figure 32. The penetration of the contact into the solder ball due to the higher temperature is greater but is well within the acceptable range. There was no visible pickup of solder on the contact tips. This experiment is being continued to evaluate the impact of longer times on the witness marks and the solder pickup. The location of the contact pinch is clearly seen in this photograph.

Figure 31. Witness Marks on Solder Ball

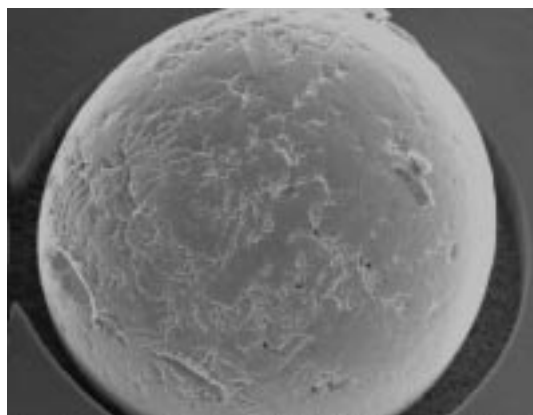
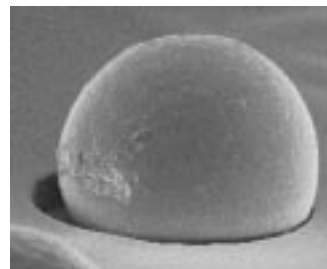


Figure 32. Effect of Burn-in on Probe Marks



Establishing Contact Force

Contact force is typically generated as a result of the deflection of the contact arm. The actual force generated is a function of the modulus of the material and the specific geometric details of the design. The solder ball diameters for CSPs tend to be small—in the range of 0.25 mm to 0.4 mm, which limits the deflection of the contact arm to a very small distance. Typically, this distance is half the ball diameter. This presents a challenge to the designer who must generate the required 15 grams of force at the contact tip, yet keep the bending stresses within the contact arms at a low enough value to achieve a 20K-cycle life. The contact force requirements are met by incorporating a pre-load, so that even for small displacements, the desired force is achieved and the socket can operate within acceptable stress levels.

The 15-gram target force is smaller than that associated with TSOP-type contact force levels, which require a 30-gram minimum. However, based on the contact tip geometry, this lower force translates to contact pressures that are high enough to achieve oxide penetration and good electrical continuity.

Conclusions and Future Work

The importance of continuing the development to 0.5-mm pitch is clear. End users want more and more electronic functionality in smaller and smaller packages. Sockets for testing these fine pitches are available today but are specialty and are considered too expensive for broad commercial application. Continued development includes innovative approaches as well as refining present methods, but at the time of the preparation of this Reference Guide, a clear-cut favorite technology had not emerged. For current progress in this and other areas of 0.5-mm-pitch technology, your local TI Field Sales representative can give you up-to-date information.

Growth rates as high as 400% for CSPs in 1998 over those in 1997 have been forecasted. The opportunity to participate in a market with this growth has provided the incentive for the socket companies to develop solutions for the infrastructure needed for burn-in test sockets. The issues of contacting the small, soft solder balls on CSPs have been solved. The price disparity between CSP sockets and TSOP sockets is to be expected during the

early days of the introduction of a new technology and is due entirely to the embryonic state of the industry and the low volume. It is believed that once this packaging technology matures and volumes increase to those of conventional burn-in sockets, then the prices for sockets for CSPs will decrease and be more in line with other commercial sockets.

6

References

K. Ano et al., "MicroStar BGAs," Application Note, TI SCJ 2328, July 1998.

Gerald Capwell, "High Density Design with MicroStar BGAs," Texas Instruments Application Note, July 1998.

James Forster, "Performance Drivers for Fine Pitch BGA Sockets," *Chip Scale Processing*, June 1998.

Kevin Lyne, "Chip Scale Packaging From Texas Instruments: MicroStar BGA," Texas Instruments Application Note, June 1997.

Gary Morrison, Les Stark, Ron Azcarte, S. Capistrano, K. Ano, K. Murata, M. Watanabe, T. Ohuchida, Y. Takahashi, Greg Ryan, "MicroStar BGA Packaging: Critical Interconnections," SEMICON '98.

Les Stark and M'hamed Idnabdeljalil, "MicroStar BGA vs. FC-CSP: Finite Element Simulation of BLR Performance: 144GGF Footprint," Texas Instruments Application Note, August 1998.

A

Frequently Asked Questions

Package Questions

Q. Do the solder balls come off during shipping?

A. No, this has never been observed. The balls are 100% inspected for coplanarity, diameter, and other physical properties prior to packing for shipment. Because solder is used during the ball-attachment process, uniformly high ball-attachment strengths are developed. Also, the ball-attachment strength is monitored frequently in the assembly process to prevent ball loss from vibration and other shipping forces.

Q. Is package repair possible? Are tools available?

A. Yes, some limited package repair is possible, and there are some semiautomatic M/C tools available. However, TI does not guarantee the reliability of repaired packages.

Q. What are the leads that appear on the package edge for? Are they connected to the inner pattern?

A. Those leads are used for plating connections during the plating of Ni/Au on the copper trace during the fabrication of the substrate. Since they do have electrical connection with the inner pattern, they can be used for test probing and signal analysis. There is no reliability risk with them.

Q. What is the composition and melting point of the solder balls?

A. The balls are a near-Sn/Pb eutectic solder that includes some additives to improve thermal fatigue life. The liquidus temperature is 178°C to 210°C.

Q. Is burn-in testing possible? How about ball damage?

A. There are commercial sockets available for 1.00-mm and 0.8-mm pitch package burn-in. Sockets for 0.5-mm pitch packages are now becoming available. Vendors include Texas Instruments, Yamaichi, Wells and Enplas. The ball damage observed falls within specified tolerances, so the testing does not affect board mount.

Q. Is tape-and-reel shipping available?

A. Tape-and-reel is the preferred method for shipping MicroStar BGA packages. Tray shipping methods are available upon customer request.

Q. What about actual market experience?

A. Since TI started production in May of 1996, well over 70 million units have been shipped. End products are primarily DSP Solutions such as wireless phones and digital camcorders where MicroStar BGA can create significant space savings. Technologies available in MicroStar BGAs include DSP, ASIC, Mixed Signal, and Linear devices.

Q. How does the packaging cost compare to QFPs?

A. CSPs are in many ways an ideal solution to cost reduction and miniaturization requirements. They offer enormous area reductions in comparison to QFPs and have increasing potential to do so without adding to system-level costs. In the best case, CSPs compete today on a cost-per-terminal basis with QFPs. For example, various CSPs from Texas Instruments are now available at cost parity with thin QFPs.

Assembly Questions

Q. What alignment accuracy is possible?

- A. Alignment accuracy for the 0.8-mm-pitch package is dependent upon board-level pad tolerance, placement accuracy, and solder ball position tolerance. Nominal ball position tolerances are specified at $\pm 80\text{ }\mu\text{m}$. These packages are self-aligning during solder reflow, so final alignment accuracy may be better than placement accuracy.

Q. Can the solder joints be inspected after reflow?

- A. Process yields of 5-ppm (parts per million) rejects are typically seen, so no final in-line inspection is required. Some customers are achieving satisfactory results during process set-up with lamographic X-ray techniques.

Q. How do the board assembly yields of MicroStar BGAs compare to QFPs?

- A. Many customers are initially concerned about assembly yields. However, once they had MicroStar BGAs in production, most of them report improved process yields compared to QFPs. This is due to the elimination of bent and misoriented leads, the wider terminal pitch than with 0.5-mm-pitch QFPs, and the ability of these packages to self-align during reflow. The collapsing solder balls also mean that the coplanarity is improved over leaded components.

Q. Are there specific recommendations for SMT processing?

- A. Texas Instruments recommends alignment with the solder balls for the CSP package, although it is possible to use the package outline for alignment. Most customers have found they do not need to change their reflow profile.

Q. Can the boards be repaired?

- A. Yes, there are rework and repair tools and profiles available. We strongly recommend that removed packages be discarded.

Q. Is TI developing a lead-free version of MicroStar BGAs?

- A. Yes, Texas Instruments is working toward eliminating lead in the solder balls to comply with lead-free environmental policies. The lead-free solder is in final evaluation. Only the solder will change, not the package structure or the mechanical dimensions. The solder system under development is based on Sn-Ag metallurgy. Check with your local TI Field Sales representative for sample availability.

Q. What size land diameter for these packages should I design on my board?

- A. Land size is the key to board-level reliability, and Texas Instruments strongly recommends following the design rules included in this bulletin.

Appendix







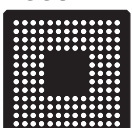

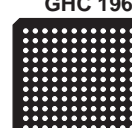


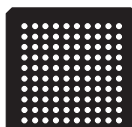
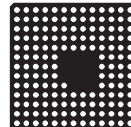



B

Package Data Sheets

Figure 33 shows TI's strategic package lineup, followed by the package data sheets for the package families offered as standard products by Texas Instruments. As new packages are added, they will be placed on the

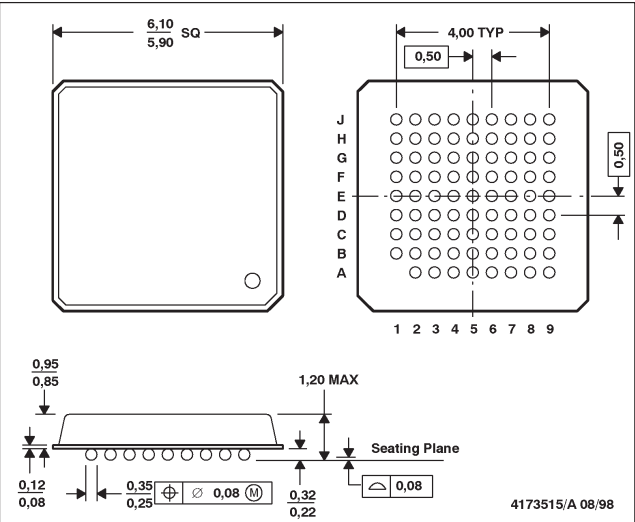
strategic package lineup. Contact your TI field sales office for information on the most current offerings. Samples are available for all packages shown in Figure 33.

Figure 33. TI's Strategic Package Line-Up

MicroStar BGA™ Package Product Guide Strategic Package Lineup: HIJI and Philippines						
PITCH (mm)	PACKAGE SIZE (mm)					
0.5	6 × 6	8 × 8	10 × 10			
	GJK 80  Qual: 4Q 99	GJJ 167  Qual: 4Q 99	GHZ 151  Qual: Complete	GGF 100  Qual: Complete		
0.8	8 × 8	10 × 10	12 × 12	15 × 15	16 × 16	
	GGV 64  Qual: Complete	GGM 80  Qual: Complete	GGU 144  Qual: Complete	GGW 176  Qual: Complete	1.0 mm PITCH GHC 196  Qual: Complete	GHK 257  Qual: Complete
	11 × 11	GGM 100	GHH 179	GGW 208	GGW 240	GJG 257
	GGT 100  Qual: Complete					
		 Qual: Complete	 Qual: Complete	 Qual: Complete	 Qual: Complete	 Qual: Complete

80GJK PACKAGE OUTLINE
(6 x 6 mm, 0.5 mm pitch)

GJK (S-PBGA-N80) PLASTIC BALL GRID ARRAY

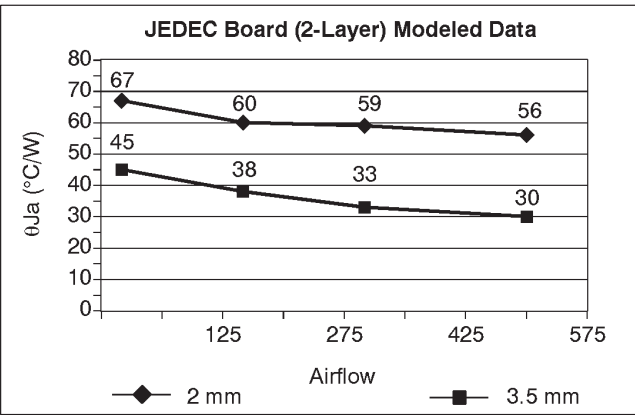


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

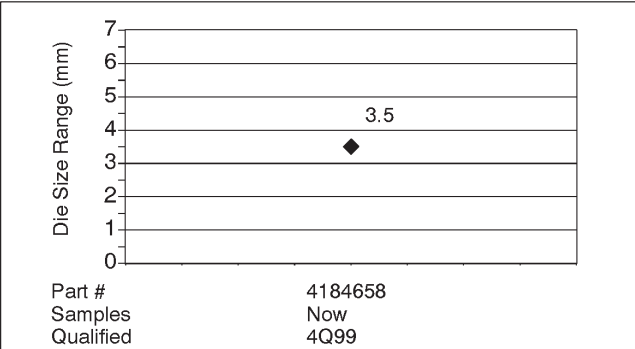
Electrical Characteristics



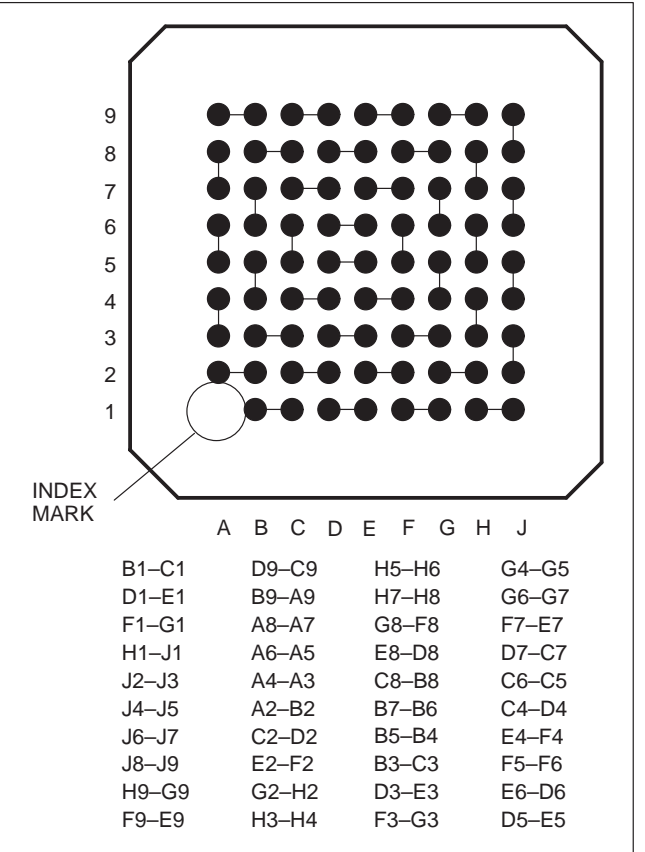
Thermal Characteristics



Productization



GJK 80 TOP VIEW DAISY CHAIN NET LIST



GJK 80 PIN ASSIGNMENT NET LIST

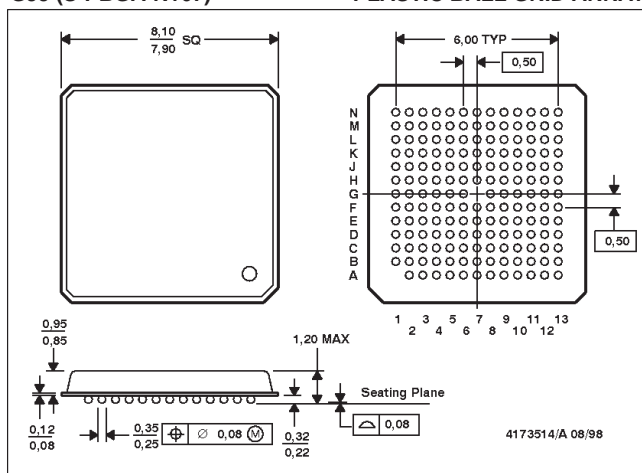
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2	B1	22	J2	42	H9	62	A8
3	D3	23	G4	43	F7	63	C6
4	E4	24	F5	44	E6	64	D5
5	C1	25	J3	45	G9	65	A7
6	D2	26	H4	46	F8	66	B6
7	E3	27	G5	47	E7	67	C5
8	D1	28	J4	48	F9	68	A6
9	E2	29	H5	49	E8	69	B5
10	F4	30	F6	50	D6	70	D4
11	E1	31	J5	51	E9	71	A5
12	F3	32	G6	52	D7	72	C4
13	F1	33	J6	53	D9	73	A4
14	F2	34	H6	54	D8	74	B4
15	G3	35	G7	55	C7	75	C3
16	G1	36	J7	56	C9	76	A3
17	G2	37	H7	57	C8	77	B3
18	H2	38	H8	58	B8	78	B2
19	H1	39	J8	59	B9	79	A2
20	J1	40	J9	60	A9	80	E5

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167GJJ PACKAGE OUTLINE (8 x 8 mm, 0.5 mm pitch)

GJJ (S-PBGA-N167)

PLASTIC BALL GRID ARRAY



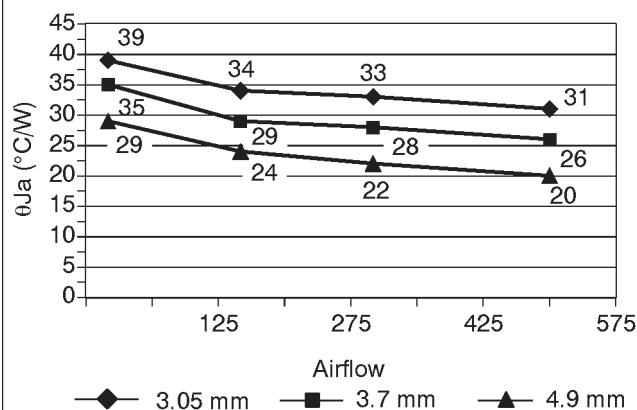
- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

Electrical Characteristics

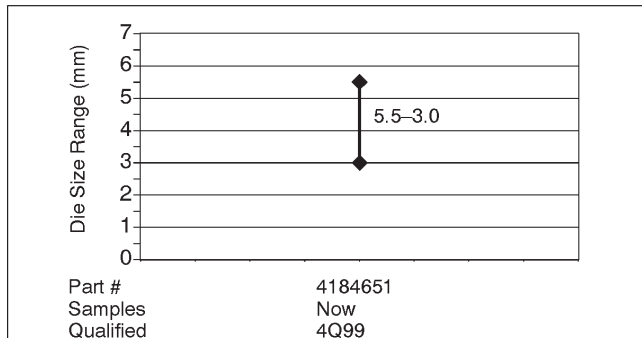
IN DEVELOPMENT

Thermal Characteristics

JEDEC Board (2-Layer) Modeled Data



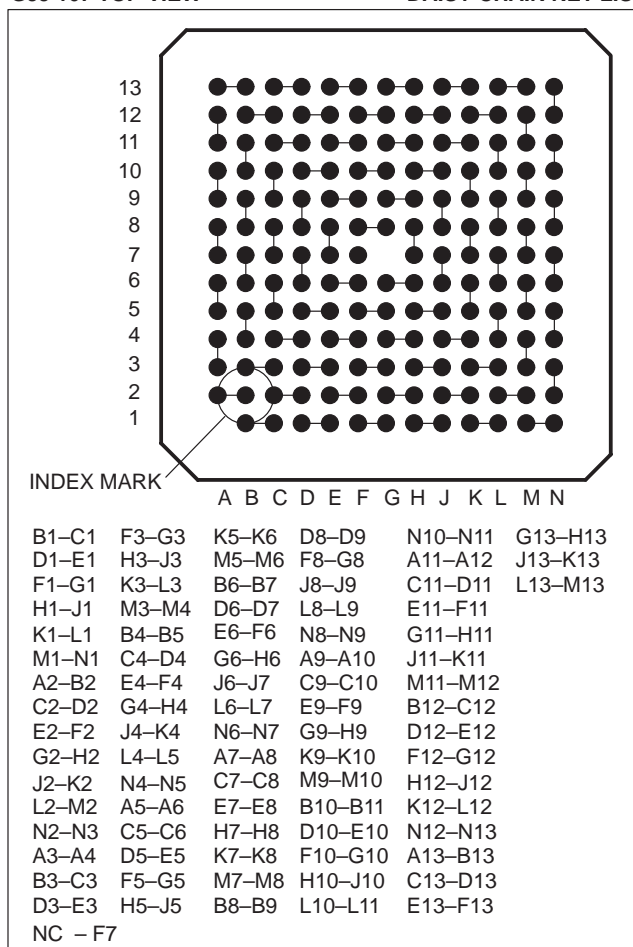
Productization



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GJJ 167 TOP VIEW

DAISY CHAIN NET LIST

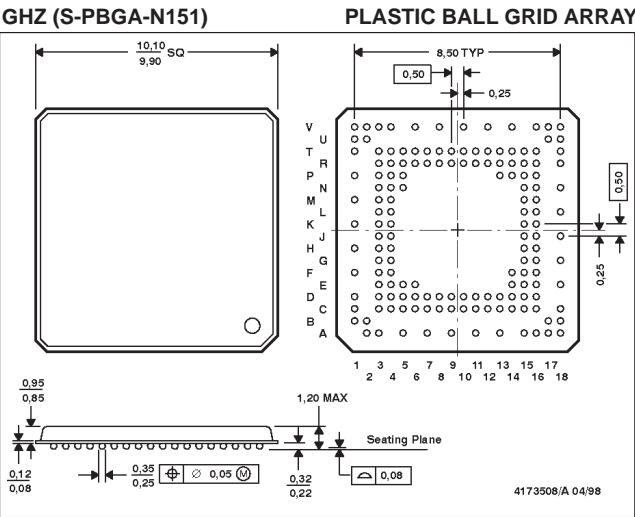


GJJ 167

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2	- D4	30	- H4	58	- M6	86	- K10	114	- F10
3	- B1	31	- K1	59	- N6	87	- M13	115	- D13
4	- C2	32	- J3	60	- H6	88	- L12	116	- E11
5	- D3	33	- K2	61	- G6	89	- K11	117	- D12
6	- E4	34	- H5	62	- N7	90	- J10	118	- F9
7	- D1	35	- L1	63	- M7	91	- L13	119	- C13
8	- D2	36	- J4	64	- L7	92	- K12	120	- E10
9	- E3	37	- L2	65	- K7	93	- J11	121	- C12
10	- D1	38	- M1	66	- N8	94	- K13	122	- B13
11	- F5	39	- K3	67	- M8	95	- H9	123	- D11
12	- E2	40	- J5	68	- J7	96	- J12	124	- E9
13	- F4	41	- M2	69	- N9	97	- H10	125	- B12
14	- E1	42	- N1	70	- L8	98	- J13	126	- A13
15	- F3	43	- L3	71	- M9	99	- H11	127	- C11
16	- F2	44	- K4	72	- K8	100	- H12	128	- D10
17	- F1	45	- N2	73	- N10	101	- H13	129	- A12
18	- F6	46	- M3	74	- L9	102	- H8	130	- B11
19	- F7	47	- L4	75	- M10	103	- H7	131	- C10
20	- G1	48	- K5	76	- J8	104	- G13	132	- D9
21	- G2	49	- N3	77	- N11	105	- G12	133	- A11
22	- G3	50	- M4	78	- K9	106	- G11	134	- B10
23	- G4	51	- L5	79	- M11	107	- G10	135	- C9
24	- H1	52	- N4	80	- N12	108	- F13	136	- A10
25	- H2	53	- J6	81	- L10	109	- F12	137	- E8
26	- G5	54	- M5	82	- J9	110	- G9	138	- B9
27	- J1	55	- K6	83	- M12	111	- E13	139	- D8
28	- H3	56	- N5	84	- N13	112	- F11	140	- A9

151GHZ PACKAGE OUTLINE
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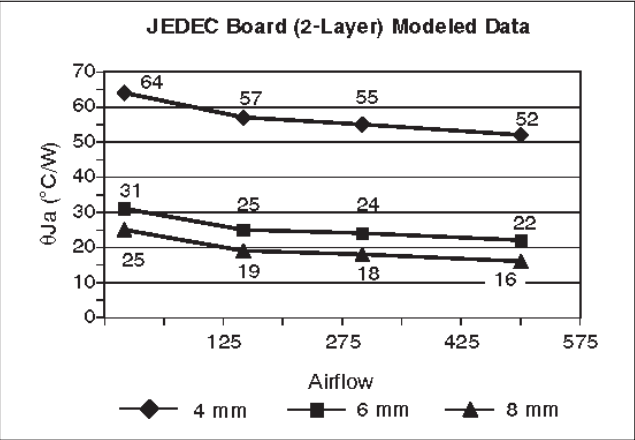


NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

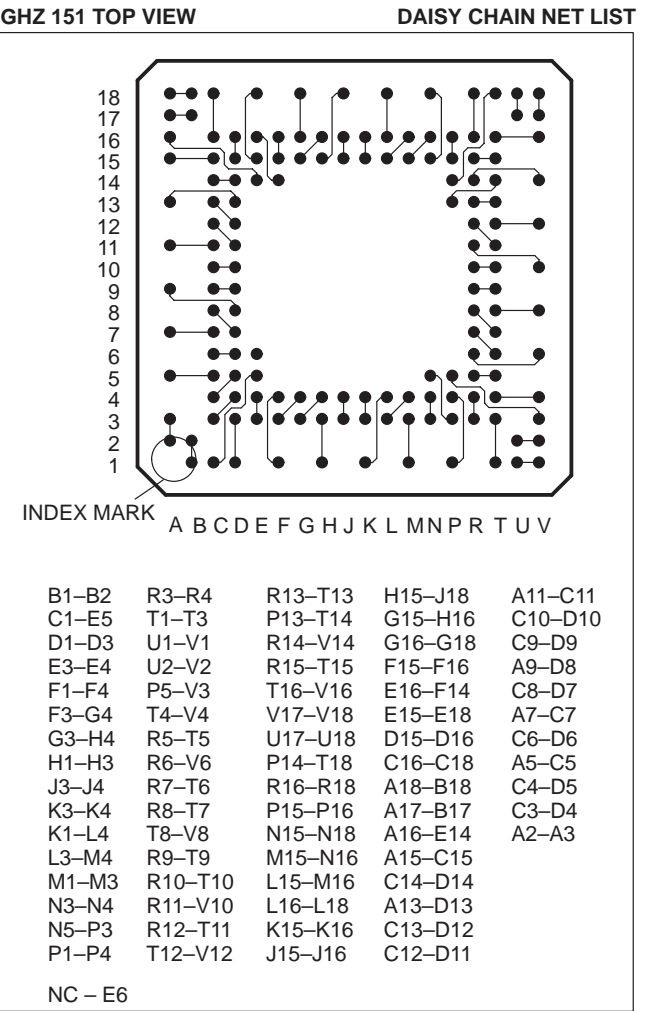
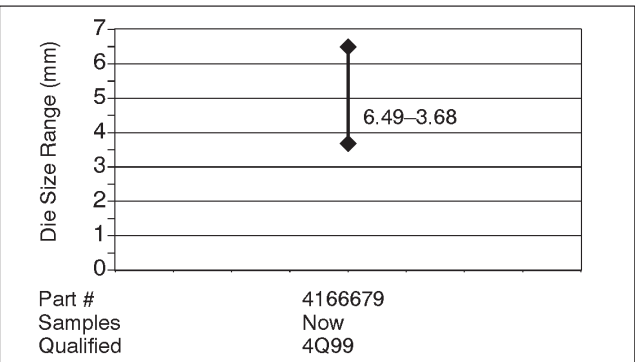
Electrical Characteristics



Thermal Characteristics



Productization



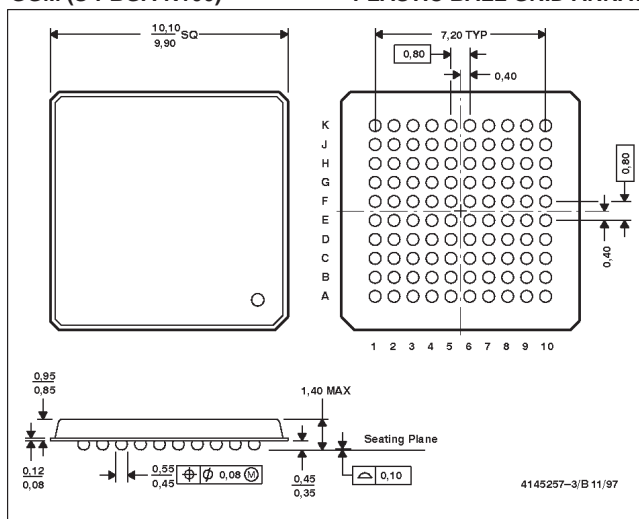
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2	B1	32	—	P4	62	—	R12	92	—	L16	122	—	C14
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4	E5	34	—	R4	64	—	V12	94	—	K16	124	—	A13
5	D1	35	—	T3	65	—	R13	95	—	J15	125	—	C13
6	D3	36	—	T1	66	—	T13	96	—	J16	126	—	D12
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9	F4	39	—	U2	69	—	V14	99	—	H16	129	—	A11
10	F1	40	—	V2	70	—	R14	100	—	G15	130	—	C11
11	F3	41	—	V3	71	—	T15	101	—	G16	131	—	D10
12	G4	42	—	P5	72	—	R15	102	—	G18	132	—	C10
13	G3	43	—	V4	73	—	T16	103	—	F15	133	—	D9
14	H4	44	—	T4	74	—	V16	104	—	F16	134	—	C9
15	H1	45	—	R5	75	—	V17	105	—	F14	135	—	A9
16	H3	46	—	T5	76	—	V18	106	—	E16	136	—	D8
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21	K1	51	—	T7	81	—	R18	111	—	C16	141	—	D6
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25	M3	55	—	R9	85	—	N15	115	—	B17	145	—	A5
26	M1	56	—	T9	86	—	N18	116	—	A17	146	—	D5
27	N4	57	—	R10	87	—	N16	117	—	A16	147	—	C4
28	N3	58	—	T10	88	—	M15	118	—	E14	148	—	D4
29	N5	59	—	V10	89	—	M16	119	—	A15	149	—	C3
30	P3	60	—	R11	90	—	L15	120	—	C15	150	—	A3
											151	—	A2

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100GGM PACKAGE OUTLINE (10 x 10 mm, 0.8 mm pitch)

GGM (S-PBGA-N100)

PLASTIC BALL GRID ARRAY

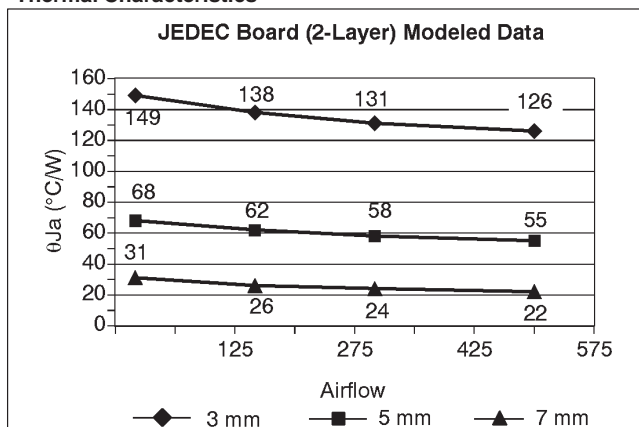


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

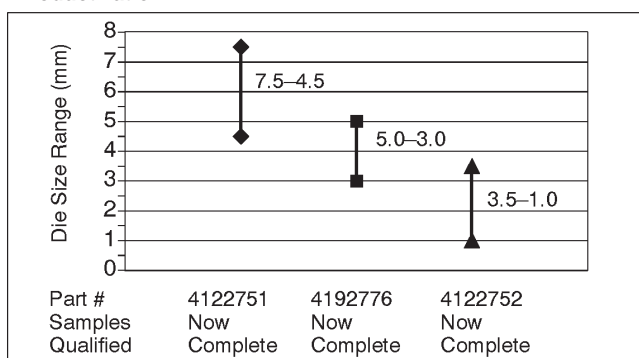
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.071	1.999	0.296
Mean	0.076	2.425	0.440
Max.	0.081	2.957	0.589

Thermal Characteristics



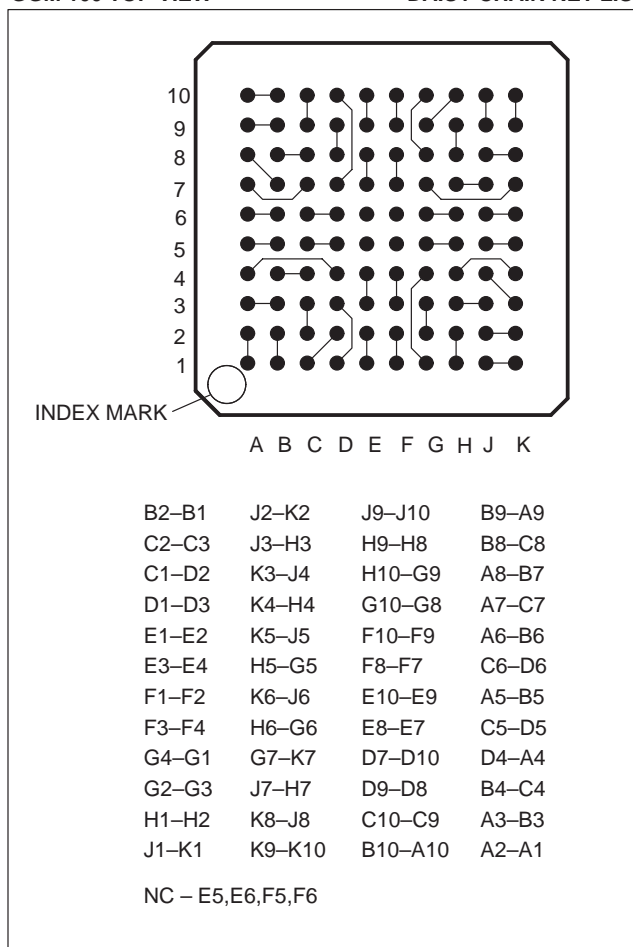
Production



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GGM 100 TOP VIEW

DAISY CHAIN NET LIST

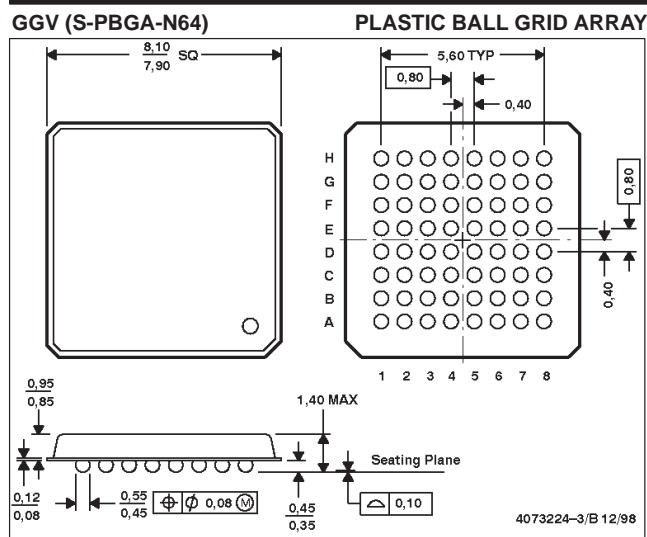


GGM 100

PIN ASSIGNMENT NET LIST

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5	C1	30	K3	55	H10	80	A8
6	D2	31	J4	56	G9	81	B7
7	D1	32	K4	57	G10	82	A7
8	D3	33	H4	58	G8	83	C7
9	E1	34	K5	59	F10	84	A6
10	E2	35	J5	60	F9	85	B6
11	E3	36	H5	61	F8	86	C6
12	E4	37	G5	62	F7	87	D6
13	E5	38	F5	63	F6	88	E6
14	F1	39	K6	64	E10	89	A5
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17	F4	42	G6	67	E7	92	D5
18	G4	43	G7	68	D7	93	D4
19	G1	44	K7	69	D10	94	A4
20	G2	45	J7	70	D9	95	B4
21	G3	46	H7	71	D8	96	C4
22	H1	47	K8	72	C10	97	A3
23	H2	48	J8	73	C9	98	B3
24	J1	49	K9	74	B10	99	A2
25	K1	50	K10	75	A10	100	A1

64GGV PACKAGE OUTLINE (8 x 8 mm, 0.8 mm pitch)

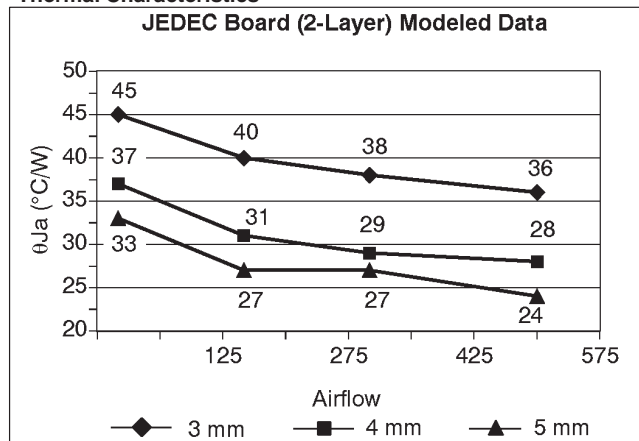


NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

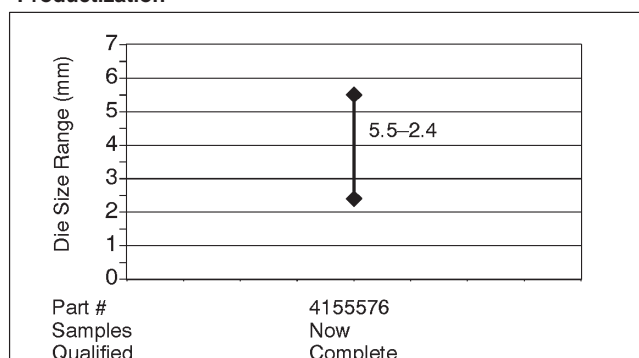
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.071	2.002	0.273
Mean	0.076	2.544	0.380
Max.	0.082	3.443	0.580

Thermal Characteristics



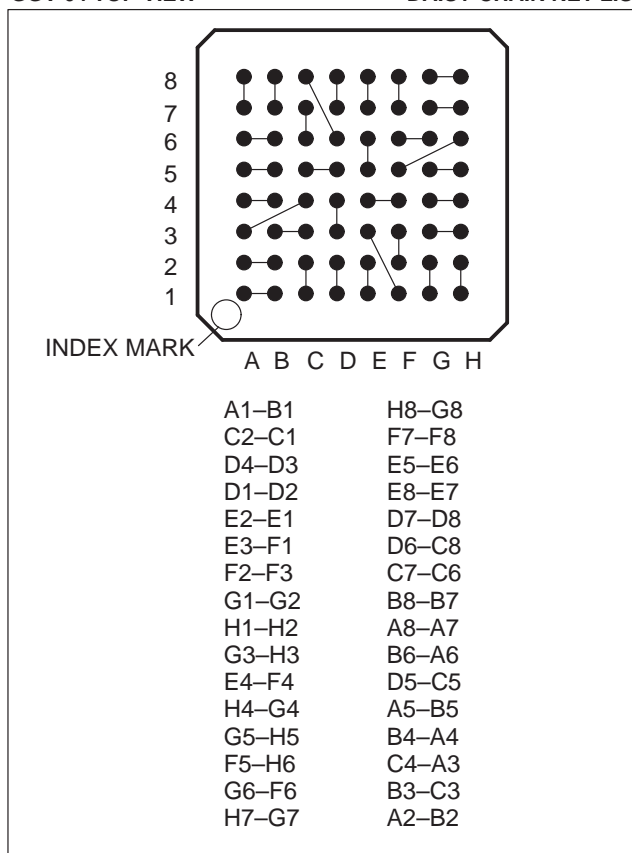
Production



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GGV 64 TOP VIEW

DAISY CHAIN NET LIST



GGV 64

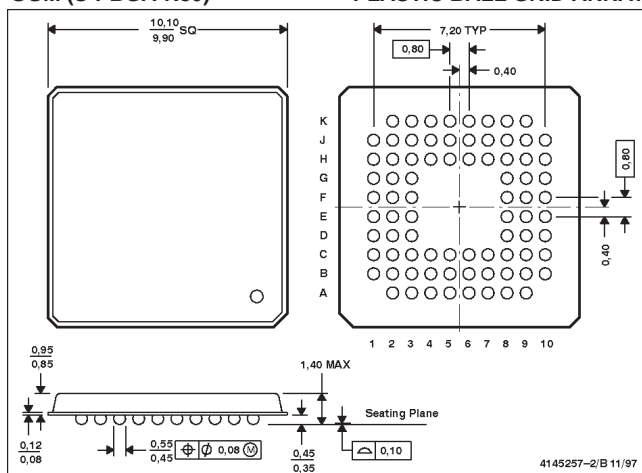
PIN ASSIGNMENT NET LIST

PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#
1 - A1	17 - H1	33 - H8	49 - A8
2 - B1	18 - H2	34 - G8	50 - A7
3 - C2	19 - G3	35 - F7	51 - B6
4 - C1	20 - H3	36 - F8	52 - A6
5 - D4	21 - E4	37 - E5	53 - D5
6 - D3	22 - F4	38 - E6	54 - C5
7 - D1	23 - H4	39 - E8	55 - A5
8 - D2	24 - G4	40 - E7	56 - B5
9 - E2	25 - G5	41 - D7	57 - B4
10 - E1	26 - H5	42 - D8	58 - A4
11 - E3	27 - F5	43 - D6	59 - C4
12 - F1	28 - H6	44 - C8	60 - A3
13 - F2	29 - G6	45 - C7	61 - B3
14 - F3	30 - F6	46 - C6	62 - C3
15 - G1	31 - H7	47 - B8	63 - A2
16 - G2	32 - G7	48 - B7	64 - B2

80GGM PACKAGE OUTLINE (10 x 10 mm, 0.8 mm pitch)

GGM (S-PBGA-N80)

PLASTIC BALL GRID ARRAY

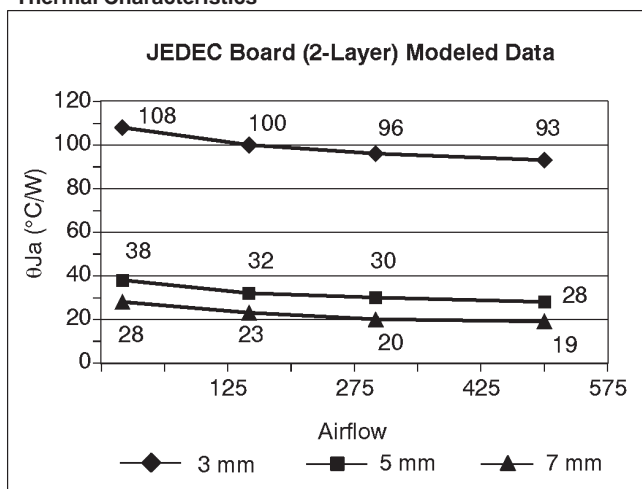


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

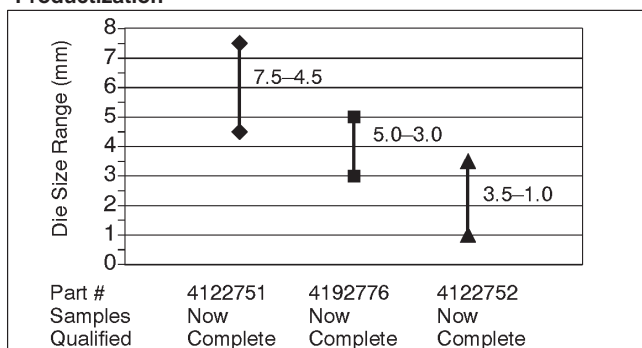
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.054	1.487	0.215
Mean	0.062	1.920	0.315
Max.	0.074	2.659	0.428

Thermal Characteristics



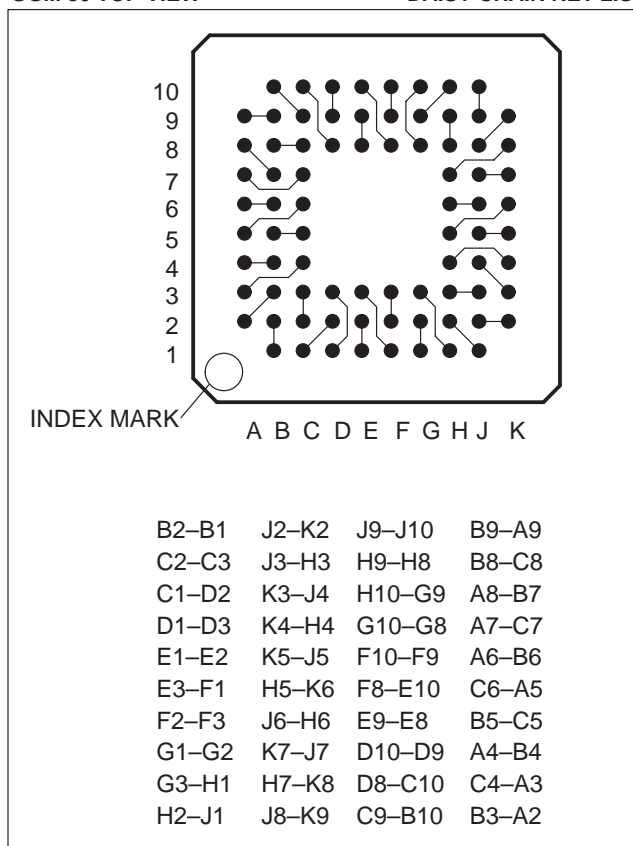
Production



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GGM 80 TOP VIEW

DAISY CHAIN NET LIST

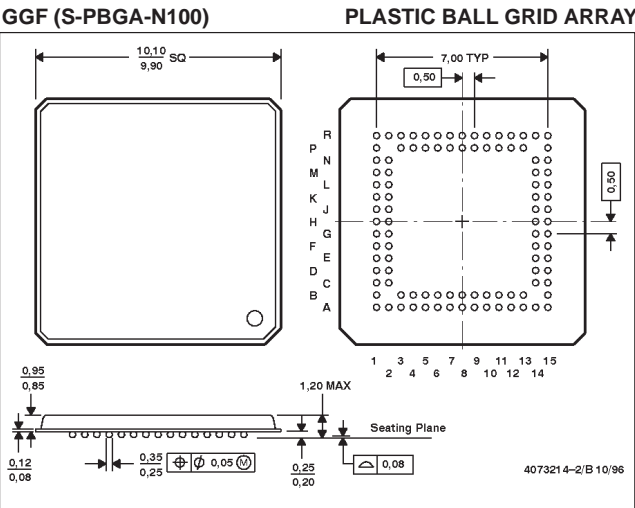


GGM 80

PIN ASSIGNMENT NET LIST

PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	B2	21	J2	41	J9	61	B9
2	B1	22	K2	42	J10	62	A9
3	C2	23	J3	43	H9	63	B8
4	C3	24	H3	44	H8	64	C8
5	C1	25	K3	45	H10	65	A8
6	D2	26	J4	46	G9	66	B7
7	D1	27	K4	47	G10	67	A7
8	D3	28	H4	48	G8	68	C7
9	E1	29	K5	49	F10	69	A6
10	E2	30	J5	50	F9	70	B6
11	E3	31	H5	51	F8	71	C6
12	F1	32	K6	52	E10	72	A5
13	F2	33	J6	53	E9	73	B5
14	F3	34	H6	54	E8	74	C5
15	G1	35	K7	55	D10	75	A4
16	G2	36	J7	56	D9	76	B4
17	G3	37	H7	57	D8	77	C4
18	H1	38	K8	58	C10	78	A3
19	H2	39	J8	59	C9	79	B3
20	J1	40	K9	60	B10	80	A2

100GGF PACKAGE OUTLINE
(10 x 10 mm, 0.5 mm pitch)

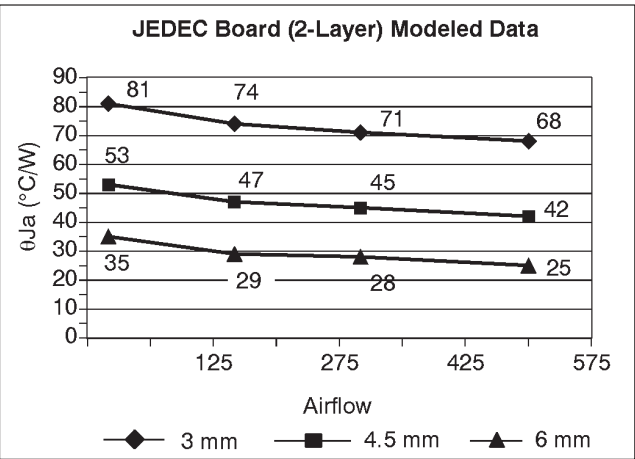


NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

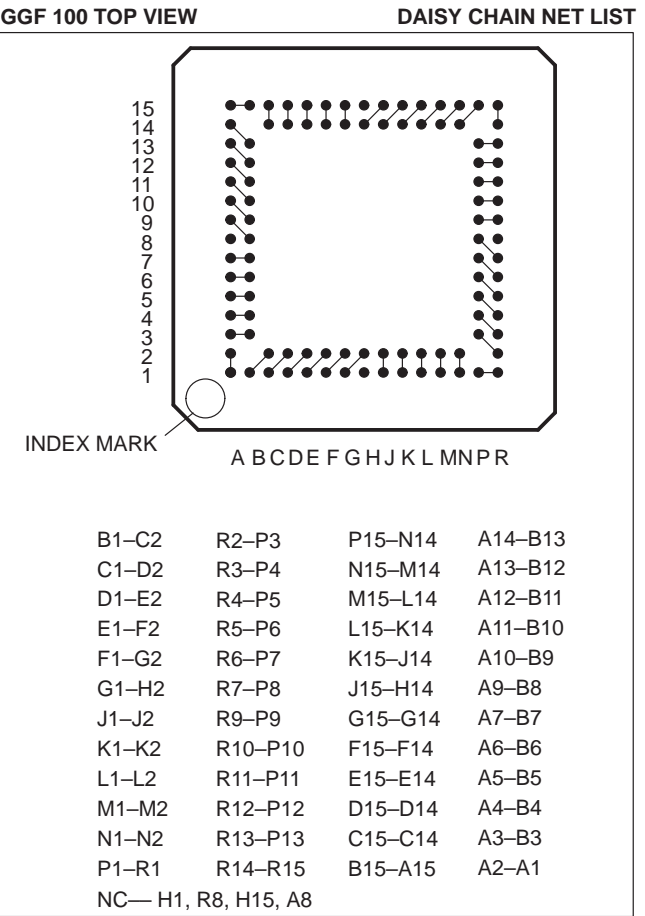
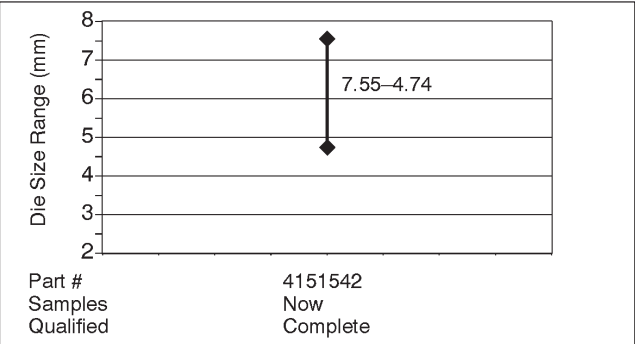
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.011	0.676	0.102
Mean	0.022	1.026	0.172
Max.	0.035	1.606	0.339

Thermal Characteristics



Production



GGF 100 PIN ASSIGNMENT NET LIST

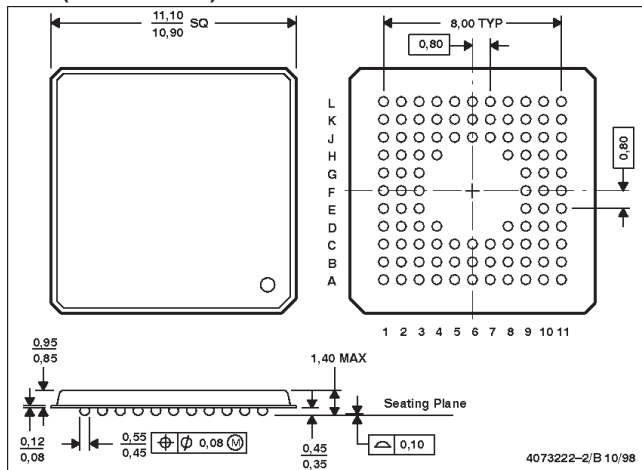
PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	B1	26	R2	51	P15	76	A14
2	C2	27	P3	52	N14	77	B13
3	C1	28	R3	53	N15	78	A13
4	D2	29	P4	54	M14	79	B12
5	D1	30	R4	55	M15	80	A12
6	E2	31	P5	56	L14	81	B11
7	E1	32	R5	57	L15	82	A11
8	F2	33	P6	58	K14	83	B10
9	F1	34	R6	59	K15	84	A10
10	G2	35	P7	60	J14	85	B9
11	G1	36	R7	61	J15	86	A9
12	H2	37	P8	62	H14	87	B8
13	H1	38	R8	63	H15	88	A8
14	J1	39	P9	64	G15	89	A7
15	J2	40	R9	65	G14	90	B7
16	K1	41	P10	66	F15	91	A6
17	K2	42	R10	67	F14	92	B6
18	L1	43	P11	68	E15	93	A5
19	L2	44	R11	69	E14	94	B5
20	M1	45	P12	70	D15	95	A4
21	M2	46	R12	71	D14	96	B4
22	N1	47	P13	72	C15	97	A3
23	N2	48	R13	73	C14	98	B3
24	P1	49	P14	74	B15	99	A2
25	R1	50	R15	75	A15	100	A1

MicroStar BGA is a trademark of Texas Instruments Incorporated.

100GGT PACKAGE OUTLINE (11 x 11 mm, 0.8 mm pitch)

GGT (S-PBGA-N100)

PLASTIC BALL GRID ARRAY

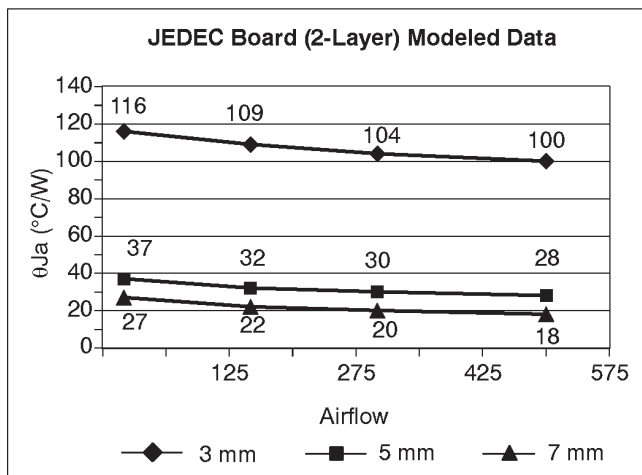


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

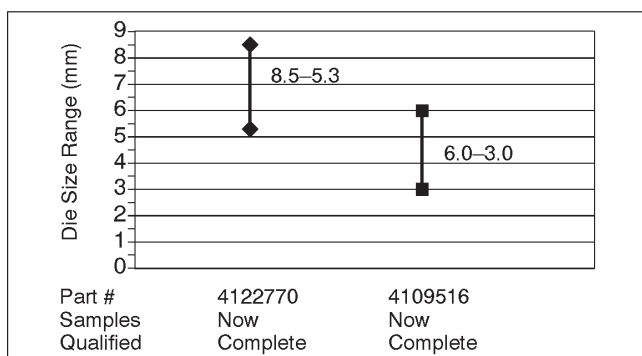
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.072	2.200	0.254
Mean	0.077	2.636	0.398
Max.	0.086	3.633	0.582

Thermal Characteristics



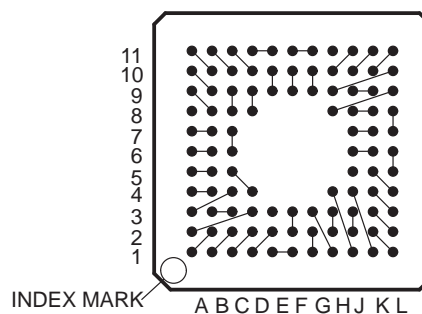
Production



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GGT 100 TOP VIEW

DAISY CHAIN NET LIST



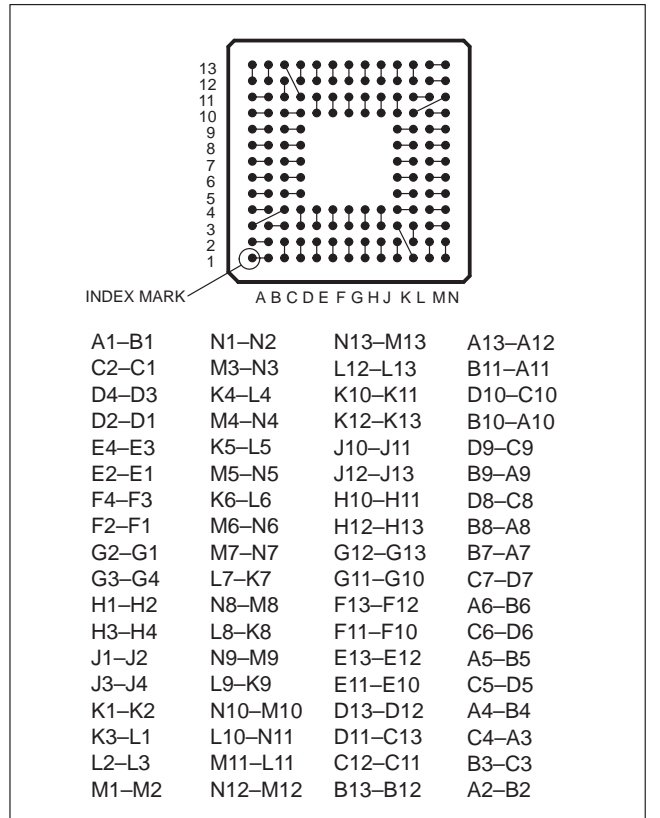
A1 — B2	L1 — K2	L11 — K10
B1 — C2	L2 — K3	K11 — J10
C1 — D2	L3 — K4	J11 — H10
D1 — E2	L4 — K5	G9 — G10
F3 — F2	J6 — K6	F9 — F10
E1 — F1	L5 — L6	G11 — F11
G1 — G2	L7 — L8	E11 — D11
G3 — H1	K7 — J7	E10 — E9
H2 — H3	K8 — J8	D10 — C11
H4 — J1	L9 — H8	D9 — D8
J2 — J3	K9 — J9	C10 — B11
K1 — J4	L10 — H9	C9 — C8
NC — E3, J5, H11, A8		

GGT 100

PIN ASSIGNMENT NET LIST

PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	— A1	26	— L1	51	— L11	76	— A11
2	— B2	27	— K2	52	— K10	77	— B10
3	— B1	28	— L2	53	— K11	78	— A10
4	— C2	29	— K3	54	— J10	79	— B9
5	— C1	30	— L3	55	— J11	80	— A9
6	— D2	31	— K4	56	— H10	81	— B8
7	— E3	32	— J5	57	— H11	82	— A8
8	— D1	33	— L4	58	— G9	83	— B7
9	— E2	34	— K5	59	— G10	84	— A7
10	— F3	35	— J6	60	— F9	85	— C7
11	— F2	36	— K6	61	— F10	86	— C6
12	— E1	37	— L5	62	— G11	87	— B6
13	— F1	38	— L6	63	— F11	88	— A6
14	— G1	39	— L7	64	— E11	89	— B5
15	— G2	40	— L8	65	— D11	90	— A5
16	— G3	41	— K7	66	— E10	91	— C5
17	— H1	42	— J7	67	— E9	92	— D4
18	— H2	43	— K8	68	— D10	93	— A4
19	— H3	44	— J8	69	— C11	94	— B4
20	— H4	45	— L9	70	— D9	95	— C4
21	— J1	46	— H8	71	— D8	96	— A3
22	— J2	47	— K9	72	— C10	97	— B3
23	— J3	48	— J9	73	— B11	98	— C3
24	— K1	49	— L10	74	— C9	99	— A2
25	— J4	50	— H9	75	— C8	100	— D3

GGU 144 TOP VIEW DAISY CHAIN NET LIST



	R (Ω)	L (nH)	C (pF)
Min.	0.052	1.438	0.215
Mean	0.055	1.958	0.305
Max.	0.062	3.095	0.563

JEDEC Board (2-Layer) Modeled Data

Airflow (L/min)	3 mm (°C/W)	5 mm (°C/W)	7 mm (°C/W)
25	122	36	25
125	114	31	21
275	109	29	19
575	105	28	18

Part #	Now (mm)	Complete (mm)
4503050	9.5	6.4
4166637	7.6	5.0
4503063	5.9	3.5

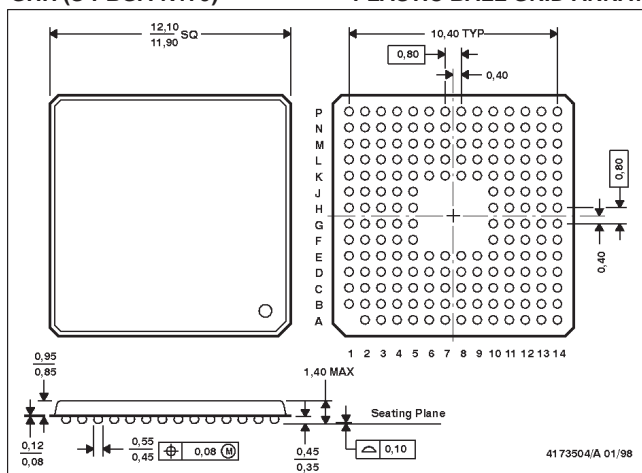
PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#
1 - A1	37 - N1	73 - N13	109 - A13
2 - B1	38 - N2	74 - M13	110 - A12
3 - C2	39 - M3	75 - L12	111 - B11
4 - C1	40 - N3	76 - L13	112 - A11
5 - D4	41 - K4	77 - K10	113 - D10
6 - D3	42 - L4	78 - K11	114 - C10
7 - D2	43 - M4	79 - K12	115 - B10
8 - D1	44 - N4	80 - K13	116 - A10
9 - E4	45 - K5	81 - J10	117 - D9
10 - E3	46 - L5	82 - J11	118 - C9
11 - E2	47 - M5	83 - J12	119 - B9
12 - E1	48 - N5	84 - J13	120 - A9
13 - F4	49 - K6	85 - H10	121 - D8
14 - F3	50 - L6	86 - H11	122 - C8
15 - F2	51 - M6	87 - H12	123 - B8
16 - F1	52 - N6	88 - H13	124 - A8
17 - G2	53 - M7	89 - G12	125 - B7
18 - G1	54 - N7	90 - G13	126 - A7
19 - G3	55 - L7	91 - G11	127 - C7
20 - G4	56 - K7	92 - G10	128 - D7
21 - H1	57 - N8	93 - F13	129 - A6
22 - H2	58 - M8	94 - F12	130 - B6
23 - H3	59 - L8	95 - F11	131 - C6
24 - H4	60 - K8	96 - F10	132 - D6
25 - J1	61 - N9	97 - E13	133 - A5
26 - J2	62 - M9	98 - E12	134 - B5
27 - J3	63 - L9	99 - E11	135 - C5
28 - J4	64 - K9	100 - E10	136 - D5
29 - K1	65 - N10	101 - D13	137 - A4
30 - K2	66 - M10	102 - D12	138 - B4
31 - K3	67 - L10	103 - D11	139 - C4
32 - L1	68 - N11	104 - C13	140 - A3
33 - L2	69 - M11	105 - C12	141 - B3
34 - L3	70 - L11	106 - C11	142 - C3
35 - M1	71 - N12	107 - B13	143 - A2
36 - M2	72 - M12	108 - B12	144 - B2

B-10

179GHH PACKAGE OUTLINE (12 x 12 mm, 0.8 mm pitch)

GHH (S-PBGA-N179)

PLASTIC BALL GRID ARRAY

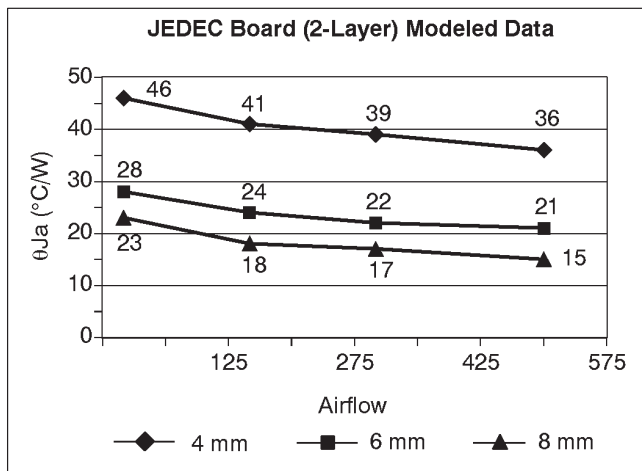


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

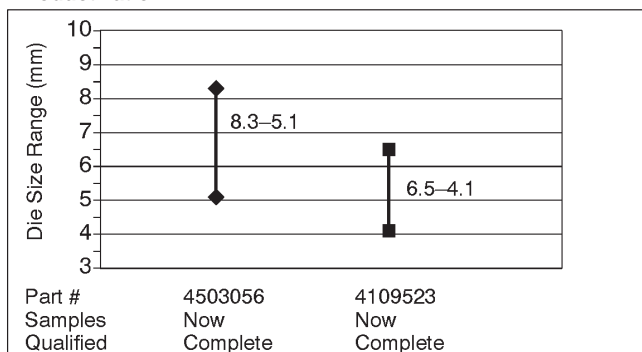
Electrical Characteristics

IN DEVELOPMENT

Thermal Characteristics



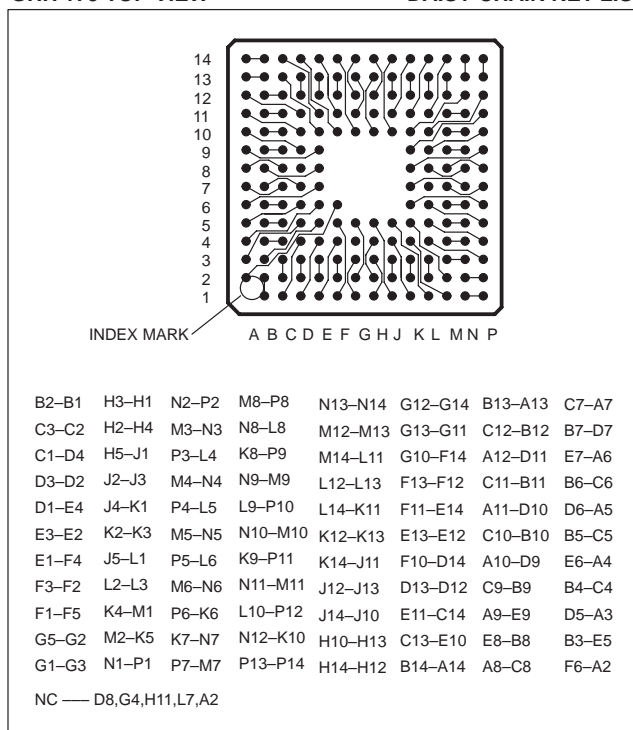
Productization



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GHH 179 TOP VIEW

DAISY CHAIN NET LIST



GHH 179

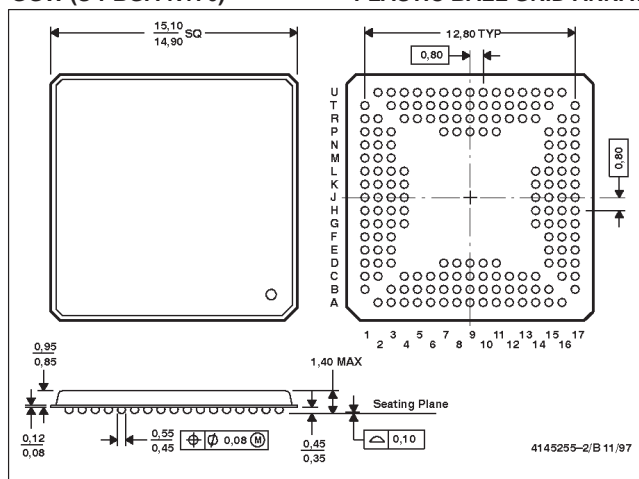
PIN ASSIGNMENT NET LIST

PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	B2	31	J3	61	N6	91	N13	121	F12
2	B1	32	J4	62	P6	92	N14	122	F11
3	C3	33	K1	63	K6	93	M12	123	E14
4	C2	34	K2	64	K7	94	M13	124	E13
5	C1	35	K3	65	N7	95	M14	125	E12
6	D4	36	J5	66	P7	96	L11	126	F10
7	D3	37	L1	67	M7	97	L12	127	D14
8	D2	38	L2	68	L7	98	L13	128	D13
9	D1	39	L3	69	M8	99	L14	129	D12
10	E4	40	K4	70	P8	100	K11	130	E11
11	E3	41	M1	71	N8	101	K12	131	C14
12	E2	42	M2	72	L8	102	K13	132	C13
13	E1	43	K5	73	K8	103	K14	133	E10
14	F4	44	N1	74	P9	104	J11	134	B14
15	F3	45	P1	75	N9	105	J12	135	A14
16	F2	46	N2	76	M9	106	J13	136	B13
17	F1	47	P2	77	L9	107	J14	137	A13
18	F5	48	M3	78	P10	108	J10	138	C12
19	G5	49	N3	79	N10	109	H10	139	B12
20	G2	50	P3	80	M10	110	H13	140	A12
21	G1	51	L4	81	K9	111	H14	141	D11
22	G3	52	M4	82	P11	112	H12	142	C11
23	G4	53	N4	83	N11	113	H11	143	B11
24	H3	54	P4	84	M11	114	G12	144	A11
25	H1	55	L5	85	L10	115	G14	145	D10
26	H2	56	M5	86	P12	116	G13	146	C10
27	H4	57	N5	87	N12	117	G11	147	B10
28	H5	58	P5	88	K10	118	G10	148	A10
29	J1	59	L6	89	P13	119	F14	149	D9
30	J2	60	M6	90	P14	120	F13	150	C9
								179	F6 (ID ball)
								180	A2

176GGW PACKAGE OUTLINE (15 x 15 mm, 0.8 mm pitch)

GGW (S-PBGA-N176)

PLASTIC BALL GRID ARRAY

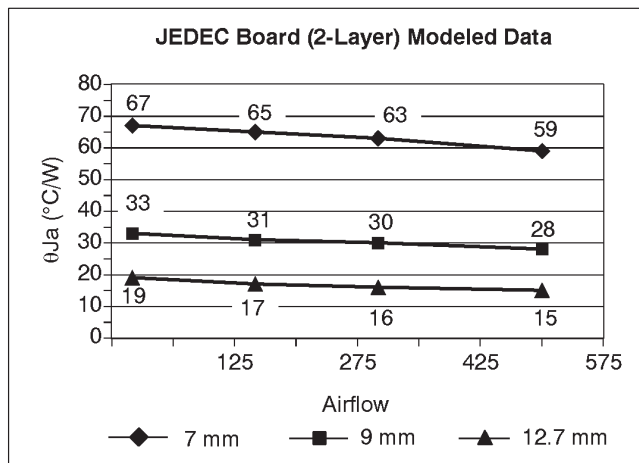


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

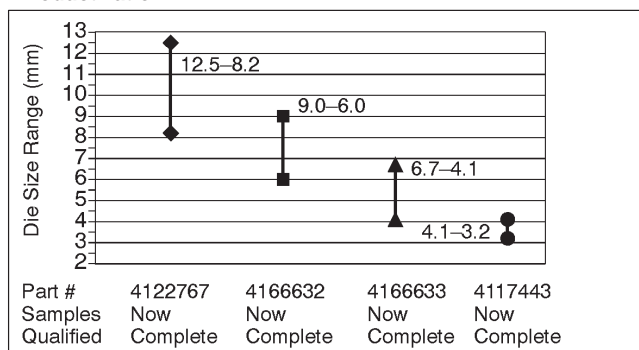
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.075	1.595	0.204
Mean	0.083	2.417	0.298
Max.	0.099	3.284	0.425

Thermal Characteristics



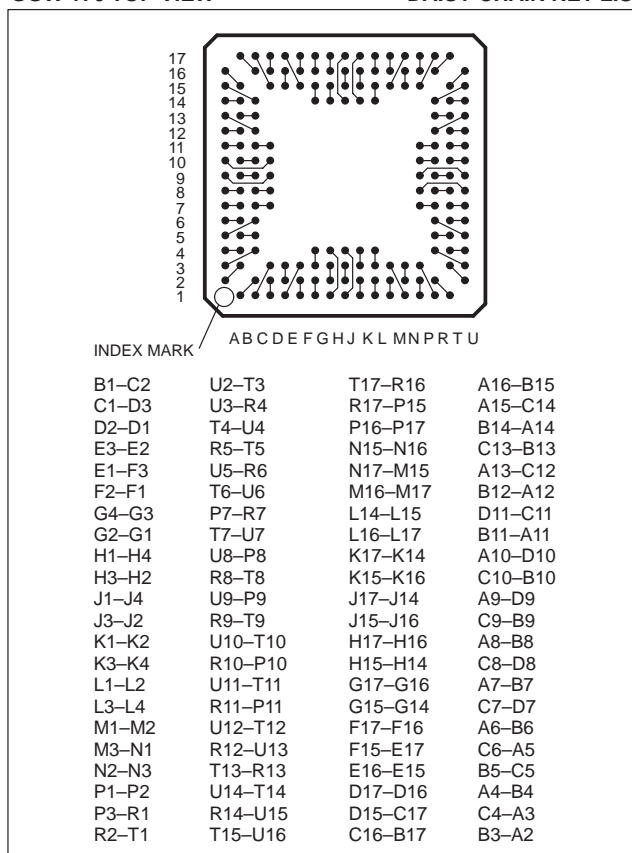
Production



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GGW 176 TOP VIEW

DAISY CHAIN NET LIST



GGW 176

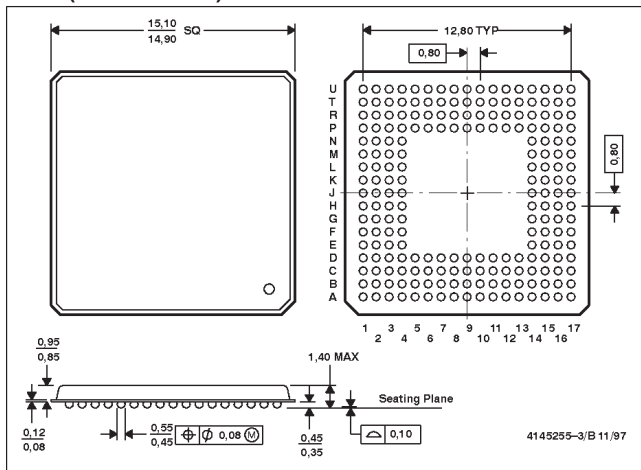
PIN ASSIGNMENT NET LIST

PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	B1	36	N1	71	P10	106	K14	141	A13
2	C2	37	N2	72	R10	107	K15	142	C12
3	C1	38	N3	73	U11	108	K16	143	B12
4	D3	39	P1	74	T11	109	J17	144	A12
5	D2	40	P2	75	R11	110	J14	145	D11
6	D1	41	P3	76	P11	111	J15	146	C11
7	E3	42	R1	77	U12	112	J16	147	B11
8	E2	43	R2	78	T12	113	H17	148	A11
9	E1	44	T1	79	R12	114	H16	149	A10
10	F3	45	U2	80	U13	115	H14	150	D10
11	F2	46	T3	81	T13	116	H15	151	C10
12	F1	47	U3	82	R13	117	G17	152	B10
13	G4	48	R4	83	U14	118	G16	153	A9
14	G3	49	T4	84	T14	119	G15	154	D9
15	G2	50	U4	85	R14	120	G14	155	C9
16	G1	51	R5	86	U15	121	F17	156	B9
17	H1	52	T5	87	T15	122	F16	157	A9
18	H4	53	U5	88	U16	123	F15	158	B8
19	H3	54	R6	89	T17	124	E17	159	D8
20	H2	55	T6	90	R16	125	E16	160	C8
21	J1	56	U6	91	R17	126	E15	161	A7
22	J4	57	P7	92	P15	127	D17	162	B7
23	J3	58	R7	93	P16	128	D16	163	C7
24	J2	59	T7	94	P17	129	D15	164	D7
25	K1	60	U7	95	N15	130	C17	165	A6
26	K2	61	U8	96	N16	131	C16	166	B6
27	K4	62	P8	97	N17	132	B17	167	C6
28	K3	63	R8	98	M15	133	A16	168	A5
29	L1	64	T8	99	M16	134	B15	169	B5
30	L2	65	U9	100	M17	135	A15	170	C5
31	L3	66	P9	101	L14	136	C14	171	A4
32	L4	67	R9	102	L15	137	B14	172	B4
33	M1	68	T9	103	L16	138	A14	173	C4
34	M2	69	U10	104	L17	139	C13	174	A3
35	M3	70	T10	105	K17	140	B13	175	B3
								176	A2

208GGW PACKAGE OUTLINE (15 x 15 mm, 0.8 mm pitch)

GGW (S-PBGA-N208)

PLASTIC BALL GRID ARRAY

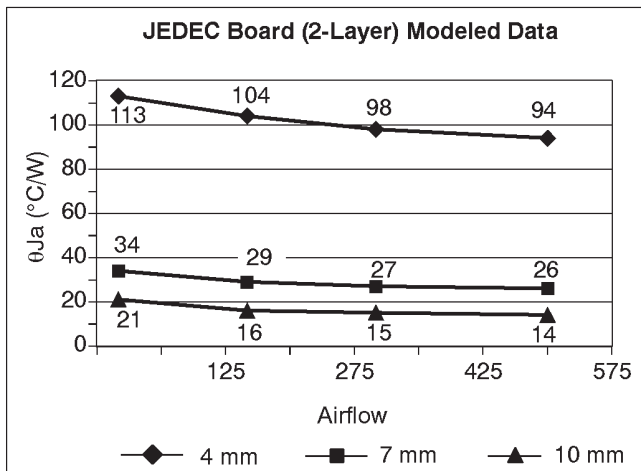


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

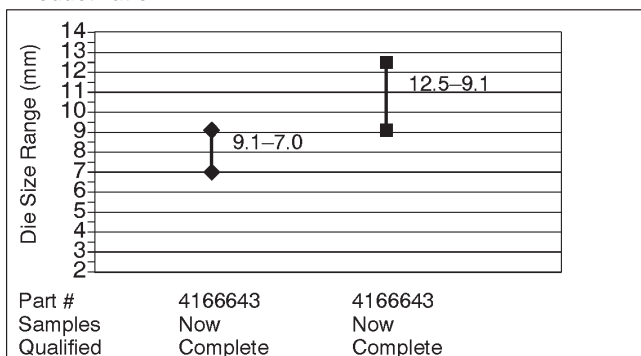
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.070	1.824	0.217
Mean	0.075	2.266	0.278
Max.	0.079	3.416	0.433

Thermal Characteristics



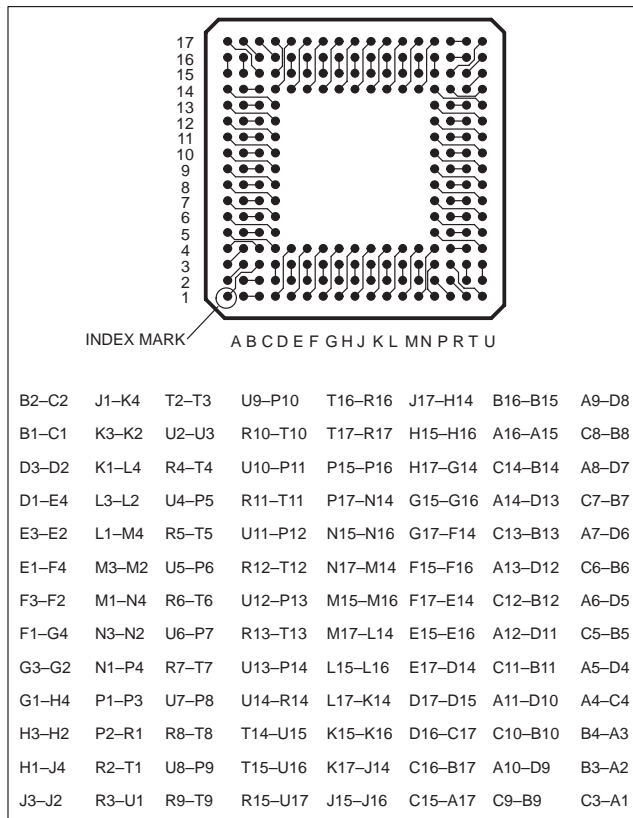
Productization



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GGW 208 TOP VIEW

DAISY CHAIN NET LIST



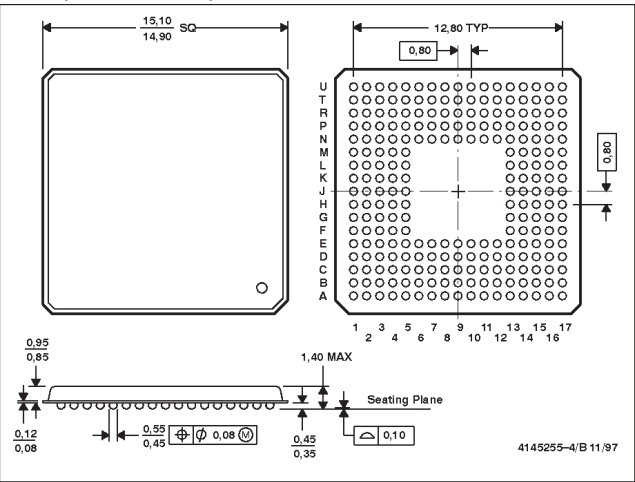
GGW 208

PIN ASSIGNMENT NET LIST

PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	— B2	27	— J1	53	— T2	79	— U9	105	— T16	131	— J17
2	— C2	28	— K4	54	— T3	80	— P10	106	— R16	132	— H14
3	— B1	29	— K3	55	— U2	81	— R10	107	— T17	133	— H15
4	— C1	30	— K2	56	— U3	82	— T10	108	— R17	134	— H16
5	— D3	31	— K1	57	— R4	83	— U10	109	— P15	135	— H17
6	— D2	32	— L4	58	— T4	84	— P11	110	— P16	136	— G14
7	— D1	33	— L3	59	— U4	85	— R11	111	— P17	137	— G15
8	— E4	34	— L2	60	— P5	86	— T11	112	— N14	138	— G16
9	— E3	35	— L1	61	— R5	87	— U11	113	— N15	139	— G17
10	— E2	36	— M4	62	— T5	88	— P12	114	— N16	140	— F14
11	— E1	37	— M3	63	— U5	89	— R12	115	— N17	141	— F15
12	— F4	38	— M2	64	— P6	90	— T12	116	— M14	142	— F16
13	— F3	39	— M1	65	— R6	91	— U12	117	— M15	143	— F17
14	— F2	40	— N4	66	— T6	92	— P13	118	— M16	144	— E14
15	— F1	41	— N3	67	— U6	93	— R13	119	— M17	145	— E15
16	— G4	42	— N2	68	— P7	94	— T13	120	— L14	146	— E16
17	— G3	43	— N1	69	— R7	95	— U13	121	— L15	147	— E17
18	— G2	44	— P4	70	— T7	96	— P14	122	— L16	148	— D14
19	— G1	45	— P1	71	— U7	97	— U14	123	— L17	149	— D17
20	— H4	46	— P3	72	— P8	98	— R14	124	— K14	150	— D15
21	— H3	47	— P2	73	— R8	99	— T14	125	— K15	151	— D16
22	— H2	48	— R1	74	— T8	100	— U15	126	— K16	152	— C17
23	— H1	49	— R2	75	— U8	101	— T15	127	— K17	153	— C16
24	— J4	50	— T1	76	— P9	102	— U16	128	— J14	154	— B17
25	— J3	51	— R3	77	— R9	103	— R15	129	— J15	155	— C15
26	— J2	52	— U1	78	— T9	104	— U17	130	— J16	156	— A17

240GGW PACKAGE OUTLINE
(15 x 15 mm, 0.8 mm pitch)

GGW (S-PBGA-N240) PLASTIC BALL GRID ARRAY

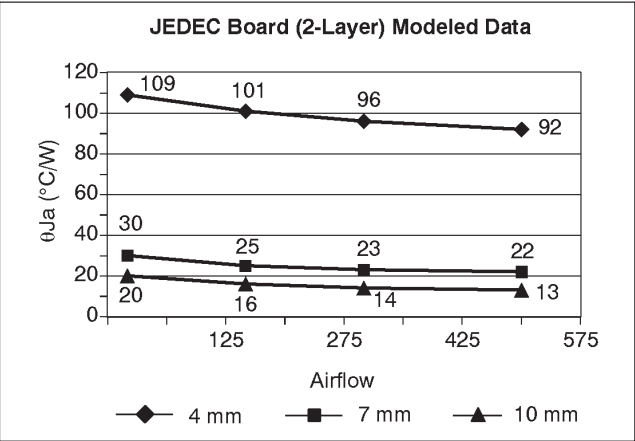


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

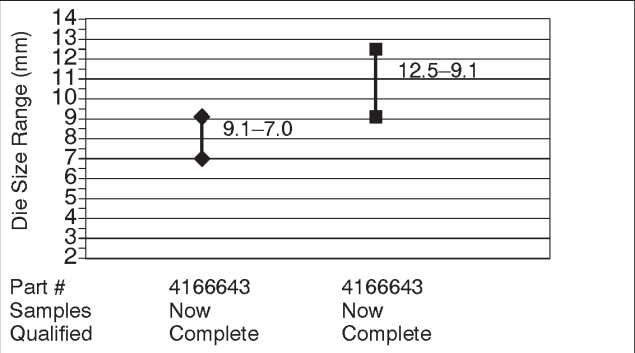
Electrical Characteristics



Thermal Characteristics

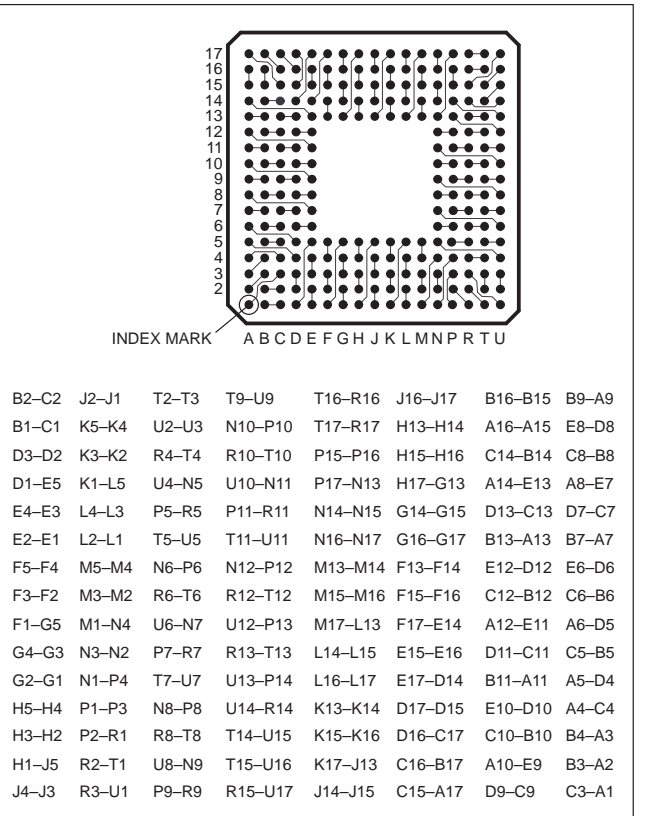


Productization



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GGW 240 TOP VIEW DAISY CHAIN NET LIST



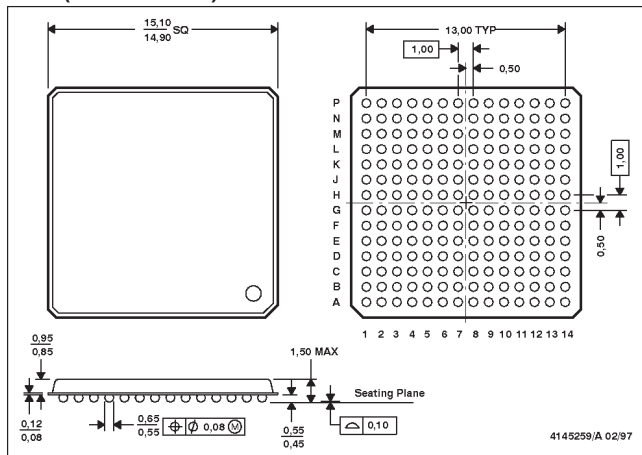
GGW 240 PIN ASSIGNMENT NET LIST

PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	B2	31	J2	61	T2	91	T9	121	T16
2	C2	32	J1	62	T3	92	U9	122	R16
3	B1	33	K5	63	U2	93	N10	123	T17
4	C1	34	K4	64	U3	94	P10	124	R17
5	D3	35	K3	65	R4	95	R10	125	P15
6	D2	36	K2	66	T4	96	T10	126	P16
7	D1	37	K1	67	U4	97	U10	127	P17
8	E5	38	L5	68	N5	98	N11	128	N13
9	E4	39	L4	69	P5	99	P11	129	N14
10	E3	40	L3	70	R5	100	R11	130	N15
11	E2	41	L2	71	T5	101	T11	131	N16
12	E1	42	L1	72	U5	102	U11	132	N17
13	F5	43	M5	73	N6	103	N12	133	M13
14	F4	44	M4	74	P6	104	P12	134	M14
15	F3	45	M3	75	R6	105	R12	135	M15
16	F2	46	M2	76	T6	106	T12	136	M16
17	F1	47	M1	77	U6	107	U12	137	M17
18	G5	48	N4	78	N7	108	P13	138	L13
19	G4	49	N3	79	P7	109	R13	139	L14
20	G3	50	N2	80	R7	110	T13	140	L15
21	G2	51	N1	81	T7	111	U13	141	L16
22	G1	52	P4	82	U7	112	P14	142	L17
23	H5	53	P1	83	N8	113	U14	143	K13
24	H4	54	P3	84	P8	114	R14	144	K14
25	H3	55	P2	85	R8	115	T14	145	K15
26	H2	56	R1	86	T8	116	U15	146	K16
27	H1	57	R2	87	U8	117	T15	147	K17
28	J5	58	T1	88	N9	118	U16	148	J13
29	J4	59	R3	89	P9	119	R15	149	J14
30	J3	60	U1	90	R9	120	U17	150	J15
								180	A17
								210	C9
								240	A1

196GHC PACKAGE OUTLINE (15 x 15 mm, 1.0 mm pitch)

GHC (S-PBGA-N196)

PLASTIC BALL GRID ARRAY

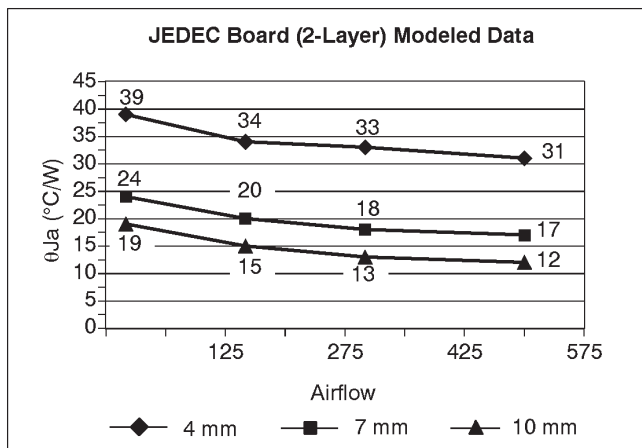


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

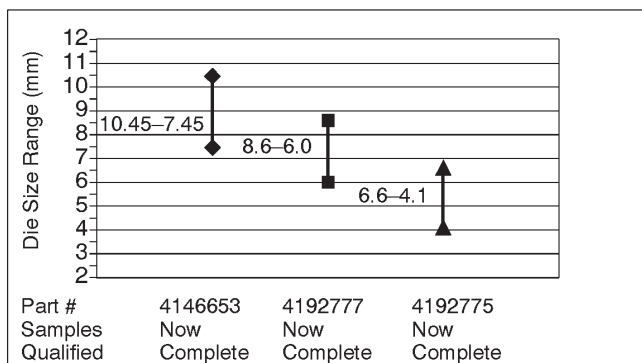
Electrical Characteristics

	R (Ω)	L (nH)	C (pF)
Min.	0.078	2.174	0.256
Mean	0.092	3.288	0.470
Max.	0.123	6.418	1.071

Thermal Characteristics



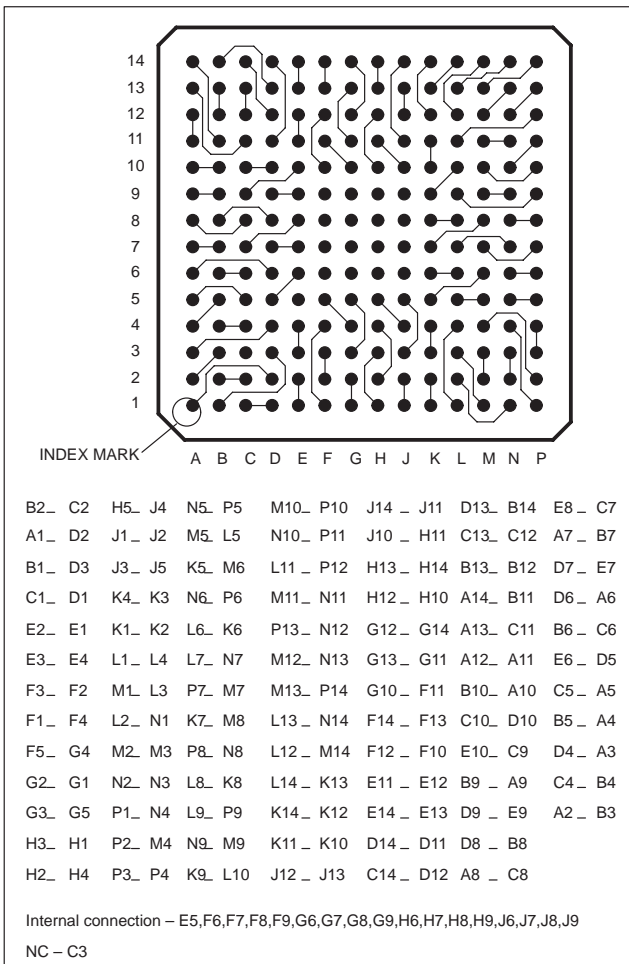
Productization



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GHC 196 TOP VIEW

DAISY CHAIN NET LIST



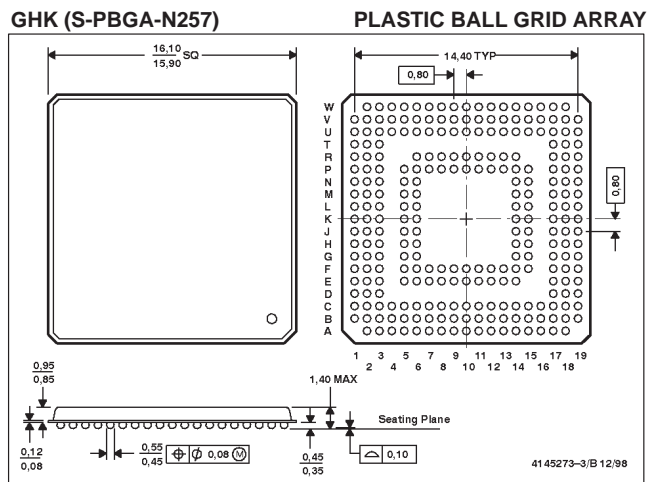
GHC 196

PIN ASSIGNMENT NET LIST

PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#	PIN#	BALL#
1	B2	27	H5	53	N5	79	M10	105	J14
2	C2	28	J4	54	P5	80	P10	106	J11
3	A1	29	J1	55	M5	81	N10	107	J10
4	D2	30	J2	56	L5	82	P11	108	H11
5	B1	31	J3	57	K5	83	L11	109	H13
6	D3	32	J5	58	M6	84	P12	110	H14
7	C1	33	K4	59	N6	85	M11	111	H12
8	D1	34	K3	60	P6	86	N11	112	H10
9	E2	35	K1	61	L6	87	P13	113	G12
10	E1	36	K2	62	K6	88	N12	114	G14
11	E3	37	L1	63	L7	89	M12	115	G13
12	E4	38	L4	64	N7	90	N13	116	G11
13	F3	39	M1	65	P7	91	M13	117	G10
14	F2	40	L3	66	M7	92	P14	118	F11
15	F1	41	L2	67	K7	93	L13	119	F14
16	F4	42	N1	68	M8	94	N14	120	F13
17	F5	43	M2	69	P8	95	L12	121	F12
18	G4	44	M3	70	N8	96	M14	122	F10
19	G2	45	N2	71	L8	97	L14	123	E11
20	G1	46	N3	72	K8	98	K13	124	E12
21	G3	47	P1	73	L9	99	K14	125	E14
22	G5	48	N4	74	P9	100	K12	126	E13
23	H3	49	P2	75	N9	101	K11	127	D14
24	H1	50	M4	76	M9	102	K10	128	D11
25	H2	51	P3	77	K9	103	J12	129	C14
26	H4	52	P4	78	L10	104	J13	130	D12
								156	C8

Internal connection - E5,F6,F7,F8,F9,G6,G7,G8,G9,H6,H7,H8,H9,J6,J7,J8,J9

257GHK PACKAGE OUTLINE (16 x 16 mm, 0.8 mm pitch)

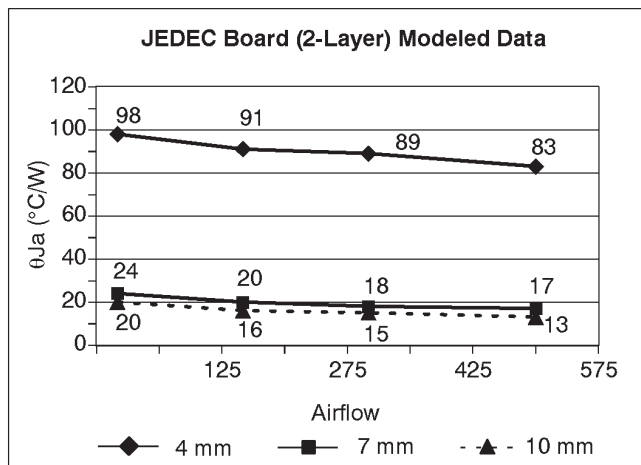


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

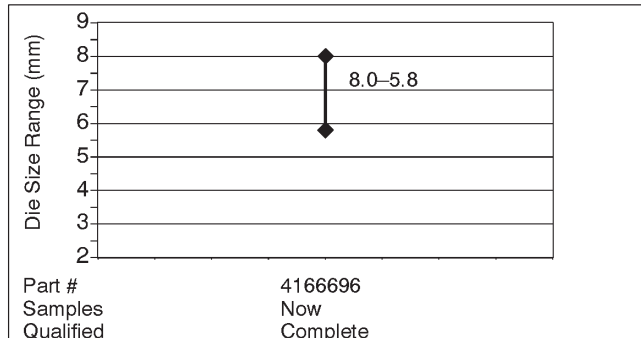
Electrical Characteristics

IN DEVELOPMENT

Thermal Characteristics



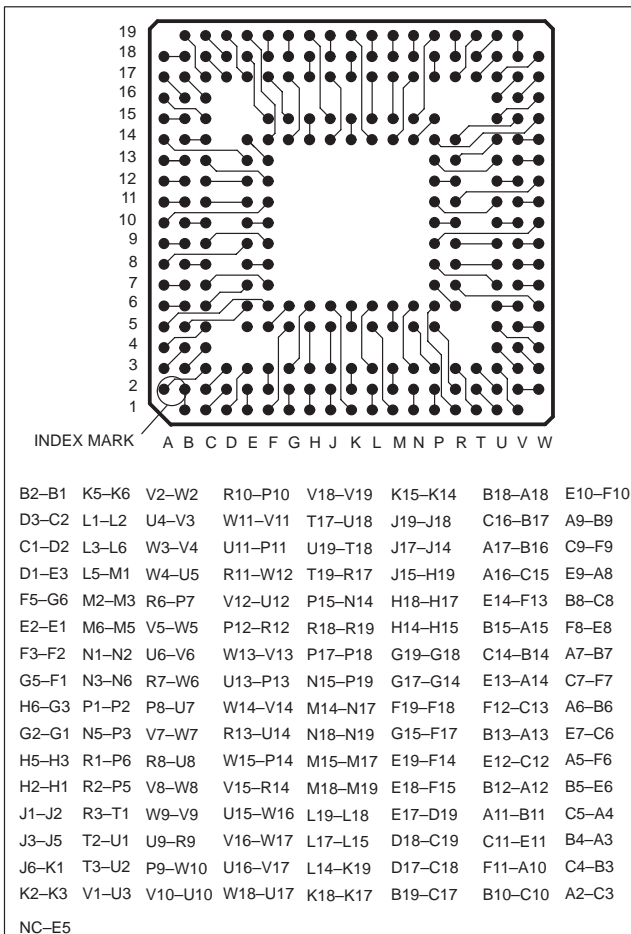
Productization



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GHK 257 TOP VIEW

DAISY CHAIN NET LIST



GHK 257

PIN ASSIGNMENT NET LIST

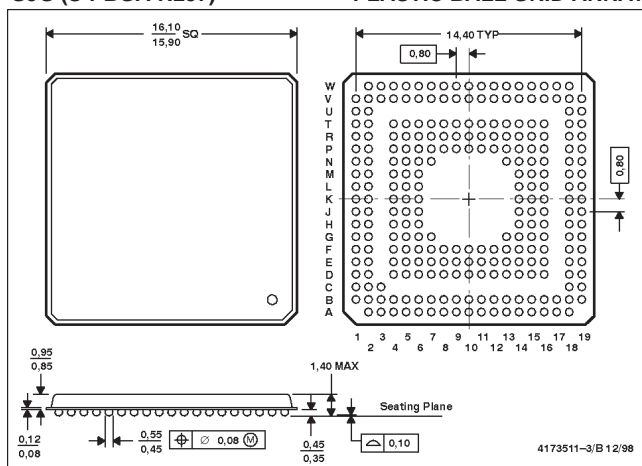
PIN#BALL#	PIN#BALL#	PIN#BALL#	PIN#BALL#	PIN#BALL#	PIN#BALL#	PIN#BALL#	PIN#BALL#
1 - B2	33 - K5	65 - V2	97 - R10	129 - V18	161 - K15	193 - B18	225 - E10
2 - B1	34 - K6	66 - W2	98 - P10	130 - V19	162 - K14	194 - A18	226 - F10
3 - D3	35 - L1	67 - U4	99 - W11	131 - T17	163 - J19	195 - C16	227 - A9
4 - C2	36 - L2	68 - V3	100 - V11	132 - U18	164 - J18	196 - B17	228 - B9
5 - C1	37 - L3	69 - W3	101 - U11	133 - U19	165 - J17	197 - A17	229 - C9
6 - D2	38 - L6	70 - V4	102 - P11	134 - T18	166 - J14	198 - B16	230 - F9
7 - D1	39 - L5	71 - W4	103 - R11	135 - T19	167 - J15	199 - A16	231 - E9
8 - E3	40 - M1	72 - U5	104 - W12	136 - R17	168 - H19	200 - C15	232 - A8
9 - F5	41 - M2	73 - R6	105 - V12	137 - P15	169 - H18	201 - E14	233 - B8
10 - G6	42 - M3	74 - P7	106 - U12	138 - N14	170 - H17	202 - F13	234 - C8
11 - E2	43 - M6	75 - V5	107 - P12	139 - R18	171 - H14	203 - B15	235 - F8
12 - E1	44 - M5	76 - W5	108 - R12	140 - R19	172 - H15	204 - A15	236 - E8
13 - F3	45 - N1	77 - U6	109 - W13	141 - P17	173 - G19	205 - C14	237 - A7
14 - F2	46 - N2	78 - V6	110 - V13	142 - P18	174 - G18	206 - B14	238 - B7
15 - G5	47 - N3	79 - R7	111 - U13	143 - N15	175 - G17	207 - E13	239 - C7
16 - F1	48 - N6	80 - W6	112 - P14	144 - P19	176 - G14	208 - A14	240 - F7
17 - H6	49 - P1	81 - P8	113 - W14	145 - M14	177 - F19	209 - F12	241 - A6
18 - G3	50 - P2	82 - U7	114 - V14	146 - N17	178 - F18	210 - C13	242 - B6
19 - G2	51 - N5	83 - V7	115 - R13	147 - N18	179 - G15	211 - B13	243 - E7
20 - G1	52 - P3	84 - W7	116 - U14	148 - N19	180 - F17	212 - A13	244 - C6
21 - H5	53 - R1	85 - R8	117 - W15	149 - M15	181 - E19	213 - E12	245 - A5
22 - H3	54 - P6	86 - U8	118 - P14	150 - M17	182 - F14	214 - C12	246 - F6
23 - H2	55 - R2	87 - V8	119 - V15	151 - M18	183 - E18	215 - B12	247 - B5
24 - H1	56 - P5	88 - W8	120 - R14	152 - M19	184 - F15	216 - A12	248 - E6
25 - J1	57 - R3	89 - W9	121 - U15	153 - L19	185 - E17	217 - A11	249 - C5
26 - J2	58 - T1	90 - V9	122 - W16	154 - L18	186 - D19	218 - B11	250 - A4
27 - J3	59 - T2	91 - U9	123 - V16	155 - L17	187 - D18	219 - C11	251 - B4
28 - J5	60 - U1	92 - R9	124 - W17	156 - L15	188 - C19	220 - E11	252 - A3
29 - J6	61 - T3	93 - P9	125 - U16	157 - L14	189 - D17	221 - F11	253 - C4
30 - K1	62 - U2	94 - W10	126 - V17	158 - K19	190 - C18	222 - A10	254 - B3
31 - K2	63 - V1	95 - V10	127 - W18	159 - K18	191 - B19	223 - B10	255 - A2
32 - K3	64 - U3	96 - U10	128 - U17	160 - K17	192 - C17	224 - C10	256 - C3

ID BALL - E5

257GJG PACKAGE OUTLINE (16 x 16 mm, 0.8 mm pitch)

GJG (S-PBGA-N257)

PLASTIC BALL GRID ARRAY

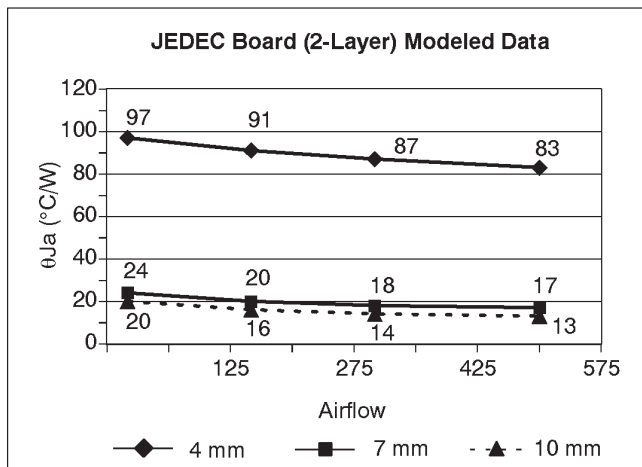


- NOTES: A. All linear dimensions are in millimeters.
B. This drawing is subject to change without notice.
C. MicroStar BGA™ configuration

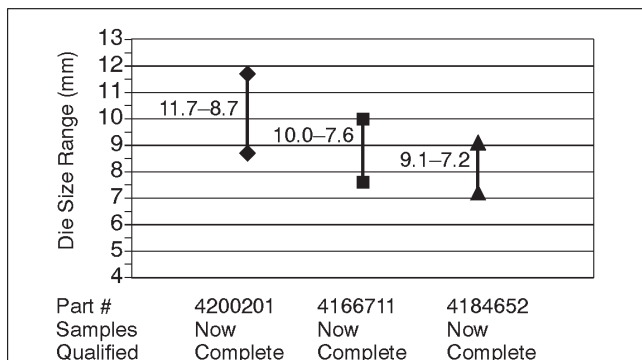
Electrical Characteristics

IN DEVELOPMENT

Thermal Characteristics



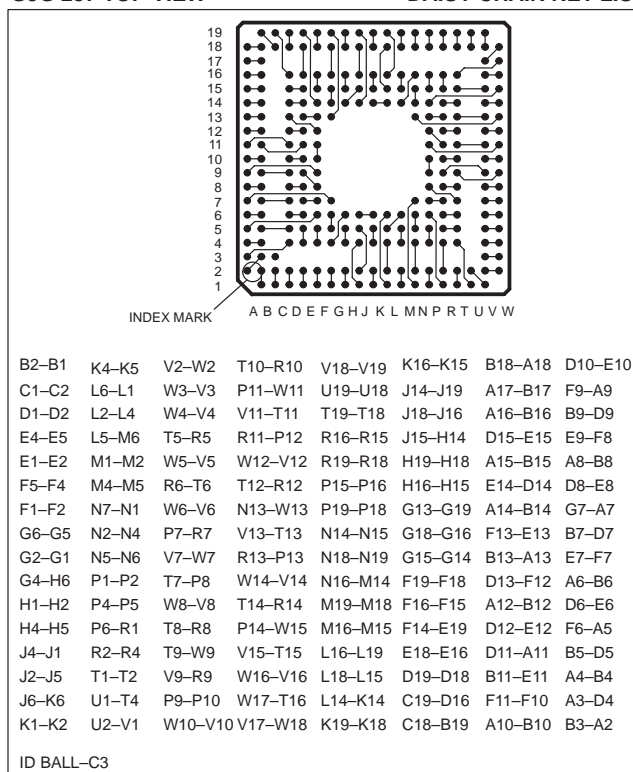
Productization



MicroStar BGA is a trademark of Texas Instruments Incorporated.

GJG 257 TOP VIEW

DAISY CHAIN NET LIST



GJG 257

PIN ASSIGNMENT NET LIST

PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#	PIN# BALL#
1 - B2	33 - K4	65 - V2	97 - T10	129 - V18	161 - K16	193 - B18	225 - D10	
2 - B1	34 - K5	66 - W2	98 - R10	130 - V19	162 - K15	194 - A18	226 - E10	
3 - C1	35 - L6	67 - W3	99 - P11	131 - U19	163 - J14	195 - A17	227 - F9	
4 - C2	36 - L1	68 - V3	100 - W11	132 - U18	164 - J19	196 - B17	228 - A9	
5 - D1	37 - L2	69 - W4	101 - V11	133 - T19	165 - J18	197 - A16	229 - B9	
6 - D2	38 - L4	70 - V4	102 - T11	134 - T18	166 - J16	198 - B16	230 - D9	
7 - E4	39 - L5	71 - T5	103 - R11	135 - R16	167 - J15	199 - D15	231 - E9	
8 - E5	40 - M6	72 - R5	104 - P12	136 - R15	168 - H14	200 - E15	232 - F8	
9 - E1	41 - M1	73 - W5	105 - W12	137 - R19	169 - H19	201 - A15	233 - A8	
10 - E2	42 - M2	74 - V5	106 - V12	138 - R18	170 - H18	202 - B15	234 - B8	
11 - F5	43 - M4	75 - R6	107 - T12	139 - P15	171 - H16	203 - E14	235 - D8	
12 - F4	44 - M5	76 - T6	108 - R12	140 - P16	172 - H15	204 - D14	236 - E8	
13 - F1	45 - N7	77 - W6	109 - N13	141 - P19	173 - G13	205 - A14	237 - G7	
14 - F2	46 - N1	78 - V6	110 - W13	142 - P18	174 - G19	206 - B14	238 - A7	
15 - G6	47 - N2	79 - P7	111 - V13	143 - N14	175 - G18	207 - F13	239 - B7	
16 - G5	48 - N4	80 - R7	112 - T13	144 - N15	176 - G16	208 - E13	240 - D7	
17 - G2	49 - N5	81 - V7	113 - R13	145 - N18	177 - G15	209 - B13	241 - E7	
18 - G1	50 - N6	82 - W7	114 - P13	146 - N19	178 - G14	210 - A13	242 - F7	
19 - G4	51 - P1	83 - T7	115 - W14	147 - N16	179 - F19	211 - D13	243 - A6	
20 - H6	52 - P2	84 - P8	116 - V14	148 - M14	180 - F18	212 - F12	244 - B6	
21 - H1	53 - P4	85 - W8	117 - T14	149 - M19	181 - F16	213 - A12	245 - D6	
22 - H2	54 - P5	86 - V8	118 - R14	150 - M18	182 - F15	214 - B12	246 - E6	
23 - H4	55 - P6	87 - T8	119 - P14	151 - M16	183 - F14	215 - D12	247 - F6	
24 - H5	56 - R1	88 - R8	120 - W15	152 - M15	184 - E19	216 - E12	248 - A5	
25 - J4	57 - R2	89 - T9	121 - V15	153 - L16	185 - E18	217 - D11	249 - B5	
26 - J1	58 - R4	90 - W9	122 - T15	154 - L19	186 - E16	218 - A11	250 - D5	
27 - J2	59 - T1	91 - V9	123 - W16	155 - L18	187 - D19	219 - B11	251 - A4	
28 - J5	60 - T2	92 - R9	124 - V16	156 - L15	188 - D18	220 - E11	252 - B4	
29 - J6	61 - U1	93 - P9	125 - W17	157 - L14	189 - C19	221 - F11	253 - A3	
30 - K6	62 - T4	94 - P10	126 - T16	158 - K14	190 - D16	222 - F10	254 - D4	
31 - K1	63 - U2	95 - W10	127 - V17	159 - K19	191 - C18	223 - A10	255 - B3	
32 - K2	64 - V1	96 - V10	128 - W18	160 - K18	192 - B19	224 - B10	256 - A2	

1PIN MARK - C3

Notes
