

POWER GOOD FAST-TRANSIENT RESPONSE 7.5-A LOW-DROPOUT VOLTAGE REGULATORS

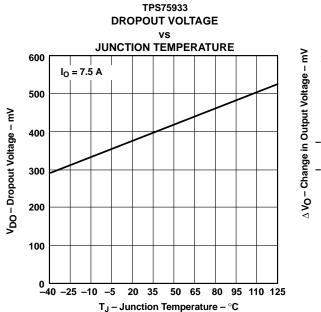
FEATURES

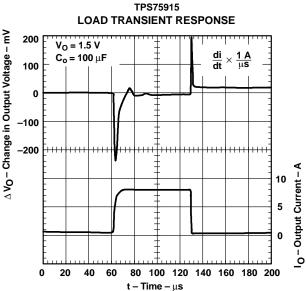
- 7.5-A Low-Dropout Voltage Regulator
- Available in 1.5-V, 1.8-V, 2.5-V, and 3.3-V
 Fixed-Output and Adjustable Versions
- Open Drain Power-Good (PG) Status Output (Fixed Options Only)
- Dropout Voltage Typically 400 mV at 7.5 A (TPS75933)
- Low 125 μA Typical Quiescent Current
- Fast Transient Response
- 3% Tolerance Over Specified Conditions for Fixed-Output Versions
- Available in 5-Pin TO-220 and TO-263 Surface-Mount Packages
- Thermal Shutdown Protection

TO-220 (KC) PACKAGE (TOP VIEW) EN < 2 IN GND 3 OUTPUT FB/PG < 5 TO-263 (KTT) PACKAGE (TOP VIEW) EN □ 1 2 IN \square GND □ 3 OUTPUT \square 4 FB/PG □ 5

DESCRIPTION

The TPS759xx family of 7.5-A low dropout (LDO) regulators contains four fixed voltage option regulators with integrated power-good (\overline{PG}) and an adjustable voltage option regulator. These devices are capable of supplying 7.5 A of output current with a dropout of 400 mV (TPS75933). Therefore, the devices are capable of performing a 3.3-V to 2.5-V conversion. Quiescent current is 125 μ A at full load and drops below 10 μ A when the devices are disabled. The TPS759xx is designed to have fast transient response for large load current changes.





A

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Because the PMOS device behaves as a low-value resistor, the dropout voltage is very low (typically 400 mV at an output current of 7.5 A for the TPS75933) and is directly proportional to the output current. Additionally, since the PMOS pass element is a voltage-driven device, the quiescent current is very low and independent of output loading (typically 125 μ A over the full range of output current, 1 mA to 7.5 A). These two key specifications yield a significant improvement in operating life for battery-powered systems.

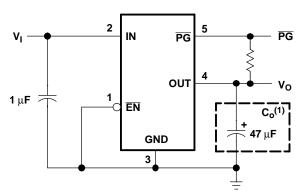
The device is enabled when \overline{EN} is connected to a low-level voltage. This LDO family also features a sleep mode; applying a TTL high signal to \overline{EN} (enable) shuts down the regulator, reducing the quiescent current to less than 1 μA at $T_J = 25$ °C. The power-good terminal (\overline{PG}) is an active low, open drain output, which can be used to implement a power-on reset or a low-battery indicator.

The TPS759xx is offered in 1.5-V, 1.8-V, 2.5-V, and 3.3-V fixed-voltage versions and in an adjustable version (programmable over the range of 1.22 V to 5 V). Output voltage tolerance is specified as a maximum of 3% over line, load, and temperature ranges. The TPS759xx family is available in a 5-pin TO-220 (KC) and TO-263 (KTT) packages.

AVAILABLE OPTIONS

T _J	OUTPUT VOLTAGE (TYP)	TO-220 (KC)	TO-263 (KTT) ⁽¹⁾
	3.3 V	TPS75933KC	TPS75933KTT
	2.5 V	TPS75925KC	TPS75925KTT
-40°C to 125°C	1.8 V	TPS75918KC	TPS75918KTT
	1.5 V	TPS75915KC	TPS75915KTT
	Adjustable 1.22 V to 5 V	TPS75901KC	TPS75901KTT

⁽¹⁾ The TPS75901 is programmable using an external resistor divider (see application information). Add **T** for KTT devices in 50-piece reel. Add **R** for KTT devices in 500-piece reel.



(1) See application information section for capacitor selection details.

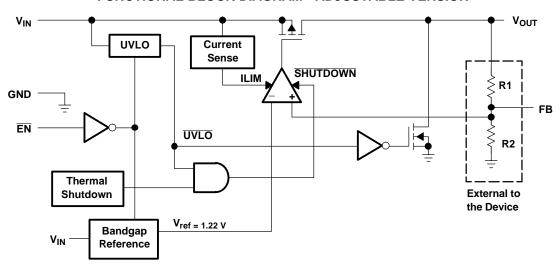
Figure 1. Typical Application Configuration (For Fixed Output Options)

Terminal Functions (TPS759xx)

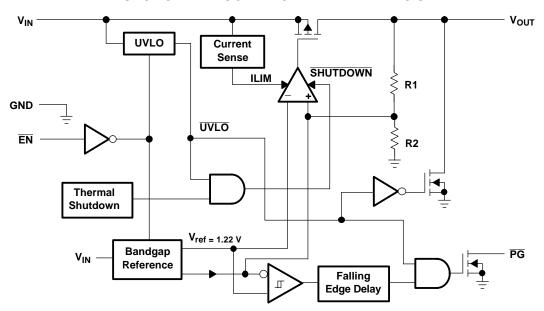
TERMINAL		I/O	DESCRIPTION				
NAME	NO.	1/0	DESCRIPTION				
EN	1	I	Enable input				
FB/PG	5	I/O	Feedback input voltage for adjustable device/PG output for fixed options				
GND	3		Regulator ground				
IN	2	I	Input voltage				
OUTPUT	4	0	Regulated output voltage				



FUNCTIONAL BLOCK DIAGRAM - ADJUSTABLE VERSION

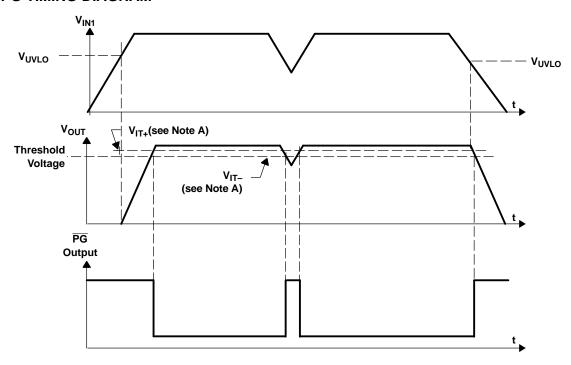


FUNCTIONAL BLOCK DIAGRAM - FIXED VERSION





TPS759xx PG TIMING DIAGRAM



NOTE A: V_{IT} –Trip voltage is typically 9% lower than the output voltage (91%V_O) V_{IT} to V_{IT} to V_{IT} is the hysteresis voltage.

DETAILED DESCRIPTION

The TPS759xx family includes four fixed-output voltage regulators (1.5 V, 1.8 V, 2.5 V, and 3.3 V), and an adjustable regulator, the TPS75901 (adjustable from 1.22 V to 5 V). The bandgap voltage is typically 1.22 V.

PIN FUNCTIONS

Enable (EN)

The \overline{EN} terminal is an input which enables or shuts down the device. If \overline{EN} is a logic high, the device will be in shutdown mode. When \overline{EN} goes to logic low, then the device will be enabled.

Power-Good (PG)

The \overline{PG} terminal for the fixed voltage option devices is an open drain, active low output that indicates the status of V_O (output of the LDO). When V_O reaches approximately 91% of the regulated voltage, \overline{PG} will go to a low impedance state. It will go to a high-impedance state when V_O falls below 91% (i.e., over load condition) of the regulated voltage. The open drain output of the \overline{PG} terminal requires a pullup resistor.

Feedback (FB)

FB is an input terminal used for the adjustable-output option and must be connected to the output terminal either directly, in order to generate the minimum output voltage of 1.22 V, or through an external feedback resistor divider for other output voltages. The FB connection should be as short as possible. It is essential to route it in such a way to minimize/avoid noise pickup. Adding RC networks between FB terminal and $V_{\rm O}$ to filter noise is not recommended because it may cause the regulator to oscillate.



Input Voltage (IN)

The V_{IN} terminal is an input to the regulator.

Output Voltage (OUTPUT)

The V_{OUTPUT} terminal is an output to the regulator.

ABSOLUTE MAXIMUM RATINGS

over operating junction temperature range (unless otherwise noted)(1)

		TPS759XX
Input voltage range ⁽²⁾	V _I	-0.3 V to 6 V
Voltage range at EN		-0.3 V to 6 V
Maximum PG voltage (TPS759xx)		6 V
Peak output current		Internally limited
Continuous total power dissipation		See Dissipation Rating Table
Output voltage	V _O (OUTPUT, FB)	5.5 V
Operating junction temperature range	T _J	-40°C to 150°C
Storage temperature range	T _{stg}	-65°C to 150°C
ESD rating	НВМ	2 kV
	CDM	500 V

⁽¹⁾ Stresses beyond those listed under absolute maximum ratings may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under recommended operating conditions is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

DISSIPATION RATING TABLE

PACKAGE	R _{⊙JC} (°C/W)	R _{⊙JA} (°C/W) ⁽¹⁾
TO-220	2	58.7 ⁽²⁾
TO-263	2	38.7 ⁽³⁾

- (1) For both packages, the $R_{\Theta JA}$ values were computed using JEDEC high K board (2S2P) with 1 ounce internal copper plane and ground plane. There was no air flow across the packages.
- (2) R_{OJA} was computed assuming a vertical, free standing TO-220 package with pins soldered to the board. There is no heatsink attached to the package.
- (3) $R_{\Theta JA}$ was computed assuming a horizontally mounted TO-263 package with pins soldered to the board. There is no copper pad underneath the package.

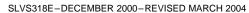
RECOMMENDED OPERATING CONDITIONS

		MIN	MAX	UNIT
V _I ⁽¹⁾	Input voltage	2.8	5.5	V
Vo	Output voltage range	1.22	5	V
Io	Output current	0	7.5	Α
TJ	Operating virtual junction temperature	-40	125	°C

⁽¹⁾ To calculate the minimum input voltage for your maximum output current, use the following equation: $V_{I(min)} = V_{O(max)} + V_{DO(max load)}$.

⁽²⁾ All voltage values are with respect to network terminal ground.

TPS75901, TPS75915 TPS75918, TPS75925, TPS75933





ELECTRICAL CHARACTERISTICS

over recommended operating junction temperature range ($T_J = -40^{\circ}C$ to 125°C), $V_I = V_{O(typ)} + 1$ V, $I_O = 1$ mA, $\overline{EN} = 0$ V, $C_O = 100 \,\mu\text{F}$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT	
		$1.22 \text{ V} \le \text{V}_{\text{O}} \le 5.5 \text{ V}, \text{T}_{\text{J}} = 25^{\circ}\text{C}$		Vo			
	Adjustable voltage	1.22 V ≤ V _O ≤ 5.5 V	0.97 V _O		1.03 V _O	V	
	rajustable voltage	1.22 V \leq V _O \leq 5.5 V, T _J = 0 to 125°C ⁽²⁾	0.98 V _O		1.02 V _O	·	
	4.5.V.Otrt	$T_J = 25^{\circ}C$, 2.8 V < $V_I < 5.5$ V		1.5			
(4)	1.5 V Output	2.8 V ≤ V _I ≤ 5.5 V	1.455		1.545	V	
Output voltage ⁽¹⁾	1.9.V. Output	$T_J = 25^{\circ}C$, 2.8 V < $V_I < 5.5$ V		1.8		V	
	1.8 V Output	$2.8 \text{ V} \le \text{V}_{\text{I}} \le 5.5 \text{ V}$	1.746	•	1.854		
	2.5.V. Output	$T_J = 25^{\circ}C, 3.5 \text{ V} < V_I < 5.5 \text{ V}$		2.5		V	
	2.5 V Output	$3.5 \text{ V} \le \text{V}_{\text{I}} \le 5.5 \text{ V}$	2.425		2.575	V	
	3.3 V Output	$T_J = 25^{\circ}C$, 4.3 V < $V_I < 5.5$ V		3.3			
	3.3 v Output	$4.3~V \leq V_I \leq 5.5~V$	3.201		3.399	V	
Quiescent current (GND cu	rrant\(3),(4)	$T_J = 25^{\circ}C$		125		μA	
Quiescent current (GND cu	ment) (***				200	μΑ	
Output voltage line regulation (ΔV _O /V _O) ⁽⁴⁾		$V_{O} + 1 \ V \le V_{I} \le 5.5 \ V, T_{J} = 25^{\circ}C$		0.04		%/V	
		$V_{O} + 1 \ V \le V_{I} < 5.5 \ V$			0.1		
Load regulation (3)				0.35		%/V	
Output noise voltage	TPS75915	BW = 300 Hz to 50 kHz, $T_J = 25^{\circ}C$, $V_I = 2.8 \text{ V}$		35		μVrms	
Output current limit	•	V _O = 0 V	8	10	14	Α	
Thermal shutdown junction	temperature			150		°C	
0. "		$\overline{\text{EN}} = \text{V}_{\text{I}}$, $\text{T}_{\text{J}} = 25^{\circ}\text{C}$		0.1		μΑ	
Standby current		$\overline{EN} = V_I$		•	10	μΑ	
FB input current	TPS75901	FB = 1.5 V	-1	•	1	μΑ	
Power supply ripple rejection	TPS75915	$f = 100 \text{ Hz}, T_J = 25^{\circ}\text{C}, V_I = 2.8 \text{ V}, I_O = 7.5 \text{ A}$		58		dB	
Minimum input voltage for v	valid PG	$I_{O(PG)} = 300 \ \mu A, \ V_{(PG)} \le 0.8 \ V$		0		V	
PG trip threshold voltage	Fixed options only	V _O decreasing	89		93	%V _O	
PGhysteresis voltage	Fixed options only	Measured at V _O		0.5		%V _O	
PGoutput low voltage	Fixed options only	V _I = 2.8 V, I _{O(PG)} = 1 mA		0.15	0.4	V	
PG leakage current	Fixed options only	V _(PG) = 5 V			1	μΑ	
Input ourrent (EN)		$\overline{EN} = V_I$	-1		1	μA	
Input current (EN)		<u>EN</u> = 0 V	-1	0	1	μA	
High level EN input voltage			2			V	
Low level EN input voltage					0.7	V	

(1)
$$I_{O} = 0$$
 mA to 7.5 A
(2) The adjustable option operates with a 2% tolerance over $T_{J} = 0$ to 125°C.
(3) $I_{O} = 0$ mA to 7.5 A
(4) If $V_{O} \le 1.8$ V then $V_{Imin} = 2.8$ V, $V_{Imax} = 5.5$ V:
Line regulator (mV) $(\%V) \times \frac{V_{O}(V_{Imax} / 2.8V)}{100} \times 1000$

If
$$V_O \ge 2.5$$
 V then $V_{Imin} = V_O + 1$ V, $V_{Imax} = 5.5$ V:
Line regulator (mV) ((%V) $\times \frac{V_O}{100} V_{Imax}$) $V_O / 1V$ $\times 1000$





over recommended operating junction temperature range ($T_J = -40^{\circ}C$ to 125°C), $V_I = V_{O(typ)} + 1$ V, $I_O = 1$ mA, $\overline{EN} = 0$ V, $C_O = 100 \mu F$ (unless otherwise noted)

PARAMETER		TEST CONDITIONS	MIN	TYP	MAX	UNIT
	Dropout voltage (3.3 V out-	$I_{O} = 7.5 \text{ A}, V_{I} = 3.2 \text{ V}, T_{J} = 25^{\circ}\text{C}$		400		mV
V_0	1) (5)	$I_O = 7.5 \text{ A}, V_I = 3.2 \text{ V}$			750	mV
	Discharge transistor current	VO = 1.5 V, T _J = 25°C	10	25		mA
V	UVLO	T _J = 25°C, V _I rising	2.2		2.75	V
V	UVLO hysteresis	T _J = 25°C, V _I falling		100		mV

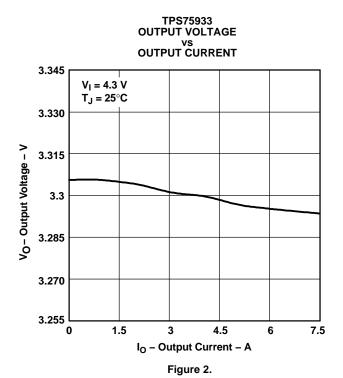
IN voltage equals V_O(Typ) - 100 mV; TPS75915, TPS75918, and TPS75925 dropout voltage limited by input voltage range limitations (i.e., TPS75933 input voltage is set to 3.2 V for the purpose of this test).

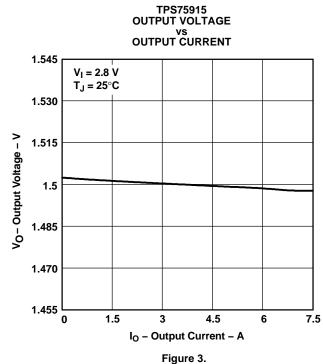


TYPICAL CHARACTERISTICS

Table of Graphs

			FIGURE
	Output valtage	vs Output current	2, 3
V _o	Output voltage	vs Junction temperature	4, 5
	Ground current	vs Junction temperature	6
	Power supply ripple rejection	vs Frequency	7
	Output spectral noise density	vs Frequency	8
z _o	Output impedance	vs Frequency	9
\/	Dranaut valtage	vs Input voltage	10
V_{DO}	Dropout voltage	vs Junction temperature	11
V _I	Minimum required input voltage	vs Output voltage	12
	Line transient response		13, 15
	Load transient response		14, 16
Vo	Output voltage and enable voltage	vs Time (start-up)	17
	Equivalent series resistance (ESR)	vs Output current	19, 20







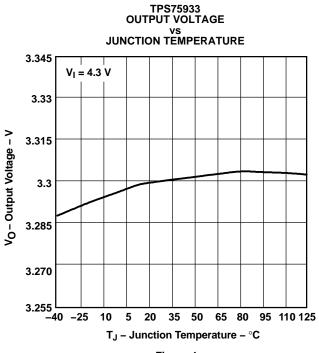


Figure 4.

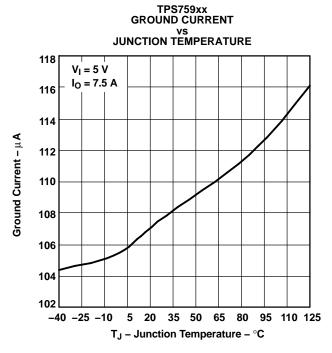


Figure 6.

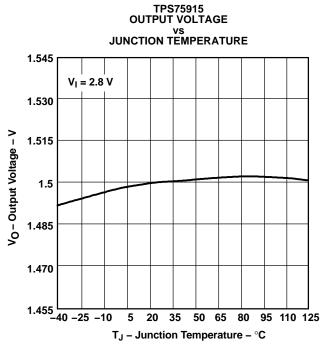


Figure 5.

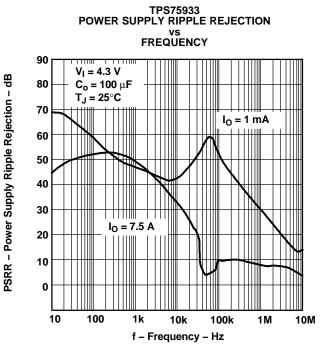
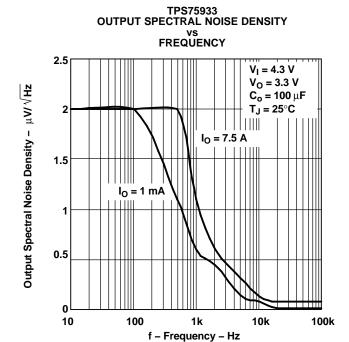
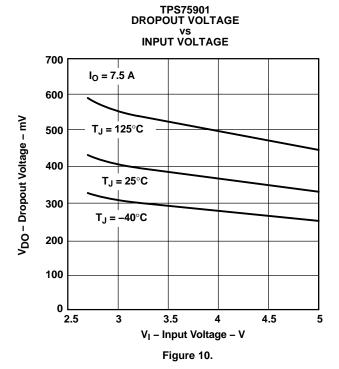


Figure 7.









TPS75933 OUTPUT IMPEDANCE VS FREQUENCY

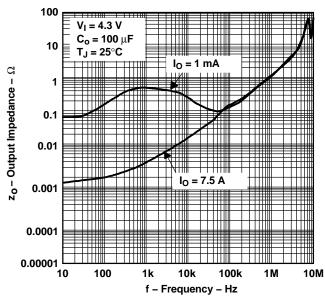


Figure 9.



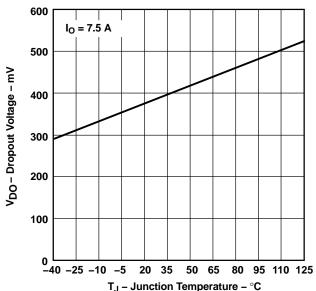
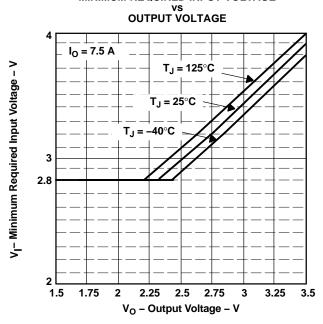


Figure 11.



MINIMUM REQUIRED INPUT VOLTAGE vs



TPS75915 LINE TRANSIENT RESPONSE

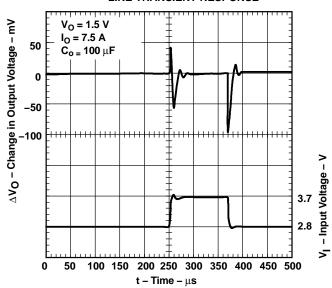


Figure 13.

TPS75915 LOAD TRANSIENT RESPONSE

Figure 12.

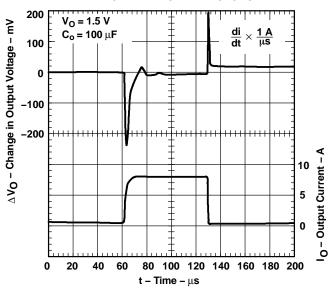


Figure 14.

TPS75933 LINE TRANSIENT RESPONSE

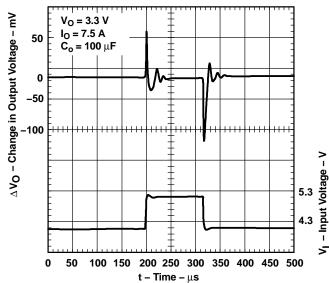


Figure 15.



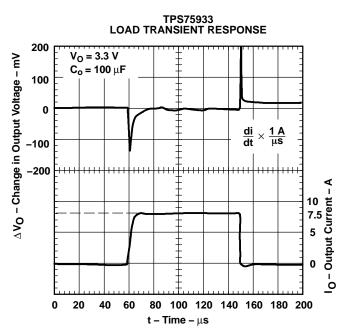
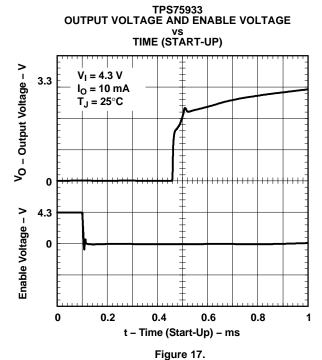


Figure 16.





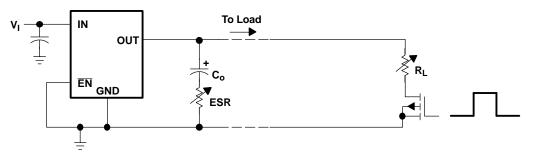
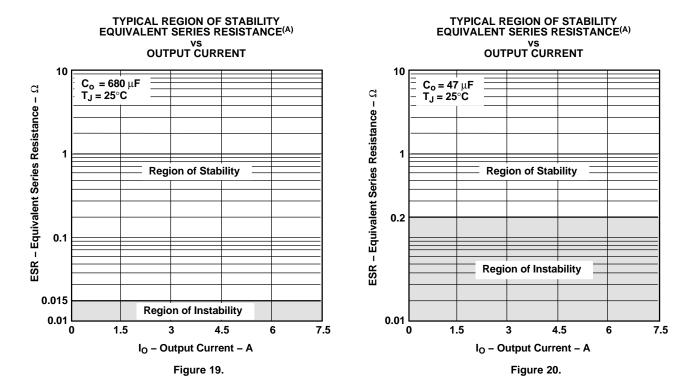


Figure 18. Test Circuit for Typical Regions of Stability (See Figure 19 and Figure 20) (Fixed Output Options)



A. Equivalent series resistance (ESR) refers to the total series resistance, including the ESR of the capacitor, ay series resistance added externally, and PWB trace resistance to C_O .



THERMAL INFORMATION

The amount of heat that an LDO linear regulator generates is directly proportional to the amount of power it dissipates during operation. All integrated circuits have a maximum allowable junction temperature (T_J max) above which normal operation is not assured. A system designer must design the operating environment so that the operating junction temperature (T_J) does not exceed the maximum junction temperature (T_J max). The two main environmental variables that a designer can use to improve thermal performance are air flow and external heatsinks. The purpose of this information is to aid the designer in determining the proper operating environment for a linear regulator that is operating at a specific power level.

In general, the maximum expected power (P_{D(max)}) consumed by a linear regulator is computed as:

$$P_{D}^{max}()V_{I(avg)} V_{O(avg)} \times I_{O(avg)} / V_{I(avg)} X_{I(Q)}$$
 (1)

Where:

- V_{I(avg)} is the average input voltage.
- V_{O(avg)} is the average output voltage.
- I_{O(avg)} is the average output current.
- I_(Q) is the quiescent current.

For most TI LDO regulators, the quiescent current is insignificant compared to the average output current; therefore, the term $V_{I(avg)}$ x $I_{(Q)}$ can be neglected. The operating junction temperature is computed by adding the ambient temperature (T_A) and the increase in temperature due to the regulator's power dissipation. The temperature rise is computed by multiplying the maximum expected power dissipation by the sum of the thermal resistances between the junction and the case $(R_{\Theta JC})$, the case to heatsink $(R_{\Theta CS})$, and the heatsink to ambient $(R_{\Theta SA})$. Thermal resistances are measures of how effectively an object dissipates heat. Typically, the larger the device, the more surface area available for power dissipation and the lower the object's thermal resistance.

Figure 21 illustrates these thermal resistances for (a) a TO-220 package attached to a heatsink, and (b) a TO-263 package mounted on a JEDEC High-K board.

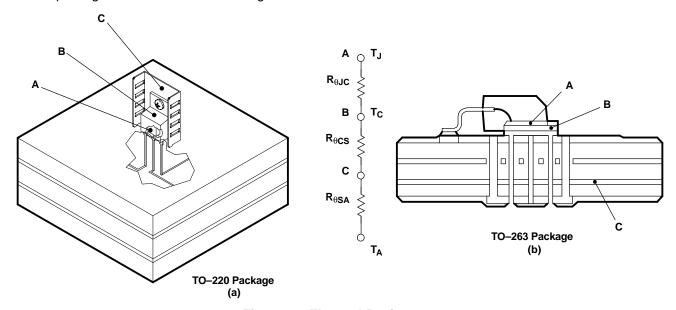


Figure 21. Thermal Resistances



Equation 2 summarizes the computation:

$$T_{J} / T_{A} \times P_{D}^{max} \times R_{\theta JC} \times R_{\theta CS} \times R_{\theta SA}$$
 (2)

The $R_{\Theta JC}$ is specific to each regulator as determined by its package, lead frame, and die size provided in the regulator's data sheet. The $R_{\Theta SA}$ is a function of the type and size of heatsink. For example, *black body radiator* type heatsinks, like the one attached to the TO-220 package in Figure 21(a), can have $R_{\Theta CS}$ values ranging from 5°C/W for very large heatsinks to 50°C/W for very small heatsinks. The $R_{\Theta CS}$ is a function of how the package is attached to the heatsink. For example, if a thermal compound is used to attach a heatsink to a TO-220 package, $R_{\Theta CS}$ of 1°C/W is reasonable.

Even if no external black body radiator type heatsink is attached to the package, the board on which the regulator is mounted will provide some heatsinking through the pin solder connections. Some packages, like the TO-263 and TI's TSSOP PowerPADTM packages, use a copper plane underneath the package or the circuit board's ground plane for additional heatsinking to improve their thermal performance. Computer aided thermal modeling can be used to compute very accurate approximations of an integrated circuit's thermal performance in different operating environments (e.g., different types of circuit boards, different types and sizes of heatsinks, different air flows, etc.). Using these models, the three thermal resistances can be combined into one thermal resistance between junction and ambient ($R_{\Theta JA}$). This $R_{\Theta JA}$ is valid only for the specific operating environment used in the computer model.

Equation 2 simplifies into Equation 3:

$$T_J / T_A \times P_D^{\text{max} \times R}_{\theta J A}$$
 (3)

Rearranging Equation 3 gives Equation 4:

$$R_{\theta JA} \times \frac{T_{J}^{-T}A}{P_{D}^{max}} \tag{4}$$

Using Equation 3 and the computer model generated curves shown in Figure 22 and Figure 25, a designer can quickly compute the required heatsink thermal resistance/board area for a given ambient temperature, power dissipation, and operating environment.

TO-220 POWER DISSIPATION

The TO-220 package provides an effective means of managing power dissipation in through-hole applications. The TO-220 package dimensions are provided in the *Mechanical Data* section at the end of the data sheet. A heatsink can be used with the TO-220 package to effectively lower the junction-to-ambient thermal resistance.

To illustrate, the TPS75925 in a TO-220 package was chosen. For this example, the average input voltage is 3.3 V, the output voltage is 2.5 V, the average output current is 3 A, the ambient temperature 55°C, the air flow is 150 LFM, and the operating environment is the same as documented below. Neglecting the quiescent current, the maximum average power is:

$$P_{D} max \times (3.3 - 2.5) V x 3 A \times 2.4 W$$
(5)

Substituting T_Jmax for T_J into Equation 4 gives Equation 6:

$$R_{\theta JA}$$
 max \times (125 – 55) °C/2.4 W \times 29 °C/W (6)

From Figure 22, $R_{\Theta JA}$ vs Heatsink Thermal Resistance, a heatsink with $R_{\Theta SA} = 22^{\circ}\text{C/W}$ is required to dissipate 2.4 W. The model operating environment used in the computer model to construct Figure 22 consisted of a standard JEDEC High-K board (2S2P) with a 1 oz. internal copper plane and ground plane. Since the package pins were soldered to the board, 450 mm² of the board was modeled as a heatsink. Figure 23 shows the side view of the operating environment used in the computer model.



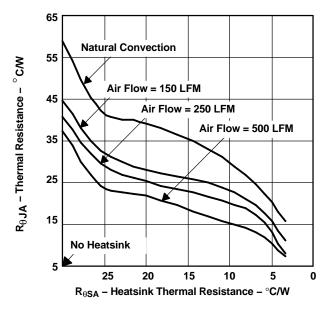
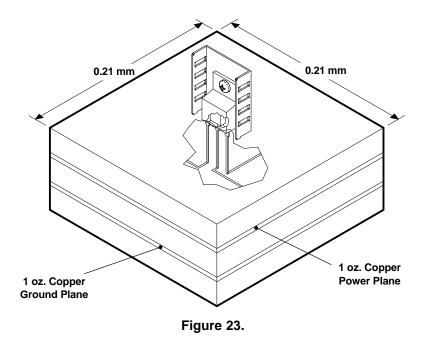


Figure 22. Thermal Resistance vs Heatsink Thermal Resistance



From the data in Figure 22 and rearranging Equation 4, the maximum power dissipation for a different heatsink $R_{\Theta SA}$ and a specific ambient temperature can be computed (see Figure 24).



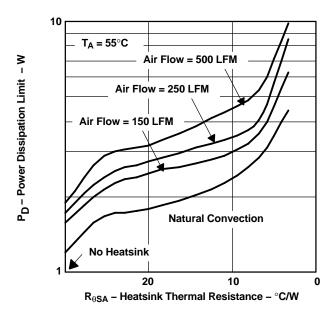


Figure 24. Power Dissipation vs Heatsink Thermal Resistance

The TO-263 package provides an effective means of managing power dissipation in surface mount applications. The TO-263 package dimensions are provided in the *Mechanical Data* section at the end of the data sheet. The addition of a copper plane directly underneath the TO-263 package enhances the thermal performance of the package.

To illustrate, the TPS75925 in a TO-263 package was chosen. For this example, the average input voltage is 3.3V, the output voltage is 2.5 V, the average output current is 3 A, the ambient temperature 55°C, the air flow is 150 LFM, and the operating environment is the same as documented below. Neglecting the quiescent current, the maximum average power is:

$$P_{D} max \times (3.3 - 2.5) V x 3 A \times 2.4 W$$
(7)

Substituting T_Jmax for T_J into Equation 4 gives Equation 8:

$$R_{\theta JA}$$
 max \times (125 – 55) °C/2.4 W \times 29 °C/W (8)

From Figure 25, $R_{\Theta JA}$ vs Copper Heatsink Area, the ground plane needs to be 2 cm² for the part to dissipate 2.4W. The model operating environment used in the computer model to construct Figure 25 consisted of a standard JEDEC High-K board (2S2P) with a 1 oz. internal copper plane and ground plane. The package is soldered to a 2 oz. copper pad. The pad is tied through thermal vias to the 1 oz. ground plane. Figure 26 shows the side view of the operating environment used in the computer model.



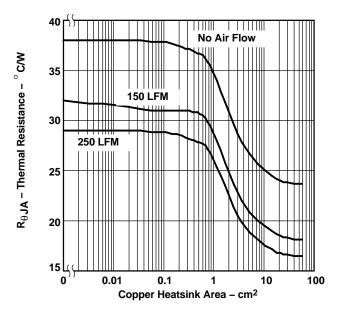


Figure 25. Thermal Resistance vs Copper Heatsink Area

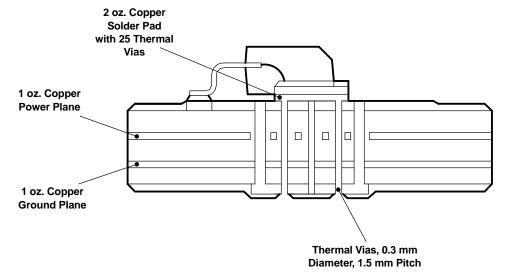


Figure 26.

From the data in Figure 25 and rearranging Equation 4, the maximum power dissipation for a different ground plane area and a specific ambient temperature can be computed (see Figure 27).



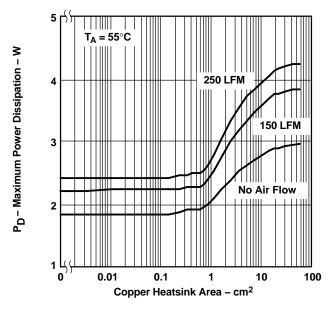


Figure 27. Maximum Power Dissipation vs Copper Heatsink Area



APPLICATION INFORMATION

PROGRAMMING THE TPS75901 ADJUSTABLE LDO REGULATOR

The output voltage of the TPS75901 adjustable regulator is programmed using an external resistor divider as shown in Figure 28. The output voltage is calculated using:

$$V_{O} V_{ref} \times \left(1 / \frac{R1}{R2}\right)$$

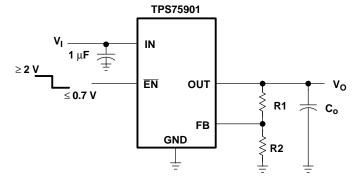
Where:

$$V_{ref} = 1.224 \text{ V}$$
 typ (the internal reference voltage)

(9)

Resistors R1 and R2 should be chosen for approximately 40- μ A divider current. Lower value resistors can be used but offer no inherent advantage and waste more power. Higher values should be avoided as leakage currents at FB increase the output voltage error. The recommended design procedure is to choose R2 = 30.1 k Ω to set the divider current at 40 μ A and then calculate R1 using:

R1
$$\left(\frac{V_O}{V_{ref}}/1\right) \times R2$$
 (10)



OUTPUT VOLTAGE PROGRAMMING GUIDE

OUTPUT VOLTAGE	R1	R2	UNIT
2.5 V	31.6	30.1	kΩ
3.3 V	51	30.1	kΩ
3.6 V	58.3	30.1	kΩ

Figure 28. TPS75901 Adjustable LDO Regulator Programming

REGULATOR PROTECTION

The TPS759xx PMOS-pass transistor has a built-in back diode that conducts reverse currents when the input voltage drops below the output voltage (e.g., during power down). Current is conducted from the output to the input and is not internally limited. When extended reverse voltage is anticipated, external limiting may be appropriate.

The TPS759xx also features internal current limiting and thermal protection. During normal operation, the TPS759xx limits output current to approximately 10 A. When current limiting engages, the output voltage scales back linearly until the overcurrent condition ends. While current limiting is designed to prevent gross device failure, care should be taken not to exceed the power dissipation ratings of the package. If the temperature of the device exceeds 150°C (typ), thermal-protection circuitry shuts it down. Once the device has cooled below 130°C (typ), regulator operation resumes.

INPUT CAPACITOR

For a typical application, a ceramic input bypass capacitor (0.22 μ F-1 μ F) is recommended to ensure device stability. This capacitor should be as close as possible to the input pin. Due to the impedance of the input supply, large transient currents will cause the input voltage to droop. If this droop causes the input voltage to drop below the UVLO threshold, the device will turn off. Therefore, it is recommended that a larger capacitor be placed in parallel with the ceramic bypass capacitor at the regulator's input. The size of this capacitor depends on the output current, response time of the main power supply, and the main power supply's distance to the regulator. At a minimum, the capacitor should be sized to ensure that the input voltage does not drop below the minimum UVLO threshold voltage during normal operating conditions.



APPLICATION INFORMATION (continued) OUTPUT CAPACITOR

As with most LDO regulators, the TPS759xx requires an output capacitor connected between OUT and GND to stabilize the internal control loop. The minimum recommended capacitance value is 47 μ F with an ESR (equivalent series resistance) of at least 200 m Ω . As shown in Figure 29, most capacitor and ESR combinations with a product of 47e-6 x 0.2 = 9.4e-6 or larger will be stable, provided the capacitor value is at least 47 μ F. Solid tantalum electrolytic and aluminum electrolytic capacitors are all suitable, provided they meet the requirements described in this section. Larger capacitors provide a wider range of stability and better load transient response.

This information along with the ESR graphs, Figure 19, Figure 20, and Figure 29, is included to assist in selection of suitable capacitance for the user's application. When necessary to achieve low height requirements along with high output current and/or high load capacitance, several higher ESR capacitors can be used in parallel to meet these guidelines.

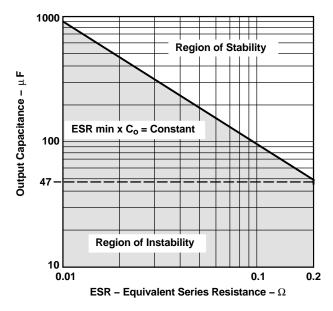


Figure 29. Output Capacitance vs Equivalent Series Resistance







PACKAGING INFORMATION

ORDERABLE DEVICE	STATUS(1)	PACKAGE TYPE	PACKAGE DRAWING	PINS	PACKAGE QTY
TPS75901KC	ACTIVE	TO/SOT	KC	5	50
TPS75901KTT	OBSOLETE	PFM	KTT	5	
TPS75901KTTR	ACTIVE	PFM	KTT	5	500
TPS75901KTTT	ACTIVE	PFM	KTT	5	50
TPS75915KC	ACTIVE	TO/SOT	KC	5	50
TPS75915KTT	OBSOLETE	PFM	KTT	5	
TPS75915KTTR	ACTIVE	PFM	KTT	5	500
TPS75915KTTT	ACTIVE	PFM	KTT	5	50
TPS75918KC	ACTIVE	TO/SOT	KC	5	50
TPS75918KTT	OBSOLETE	PFM	KTT	5	
TPS75918KTTR	ACTIVE	PFM	KTT	5	500
TPS75918KTTT	ACTIVE	PFM	KTT	5	50
TPS75925KC	ACTIVE	TO/SOT	KC	5	50
TPS75925KTT	OBSOLETE	PFM	KTT	5	
TPS75925KTTR	ACTIVE	PFM	KTT	5	500
TPS75925KTTT	ACTIVE	PFM	KTT	5	50
TPS75933KC	ACTIVE	TO/SOT	KC	5	50
TPS75933KTT	OBSOLETE	PFM	KTT	5	
TPS75933KTTR	ACTIVE	PFM	KTT	5	500
TPS75933KTTT	ACTIVE	PFM	KTT	5	50

(1) The marketing status values are defined as follows: **ACTIVE:** Product device recommended for new designs.

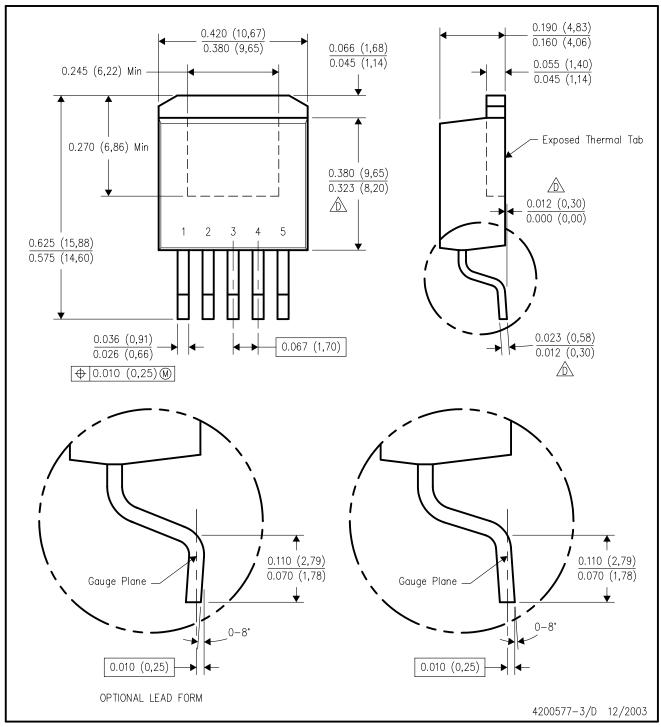
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

PREVIEW: Device has been announced but is not in production. Samples may or may not be available. **OBSOLETE:** TI has discontinued the production of the device.

KTT (R-PSFM-G5)

PLASTIC FLANGE-MOUNT PACKAGE

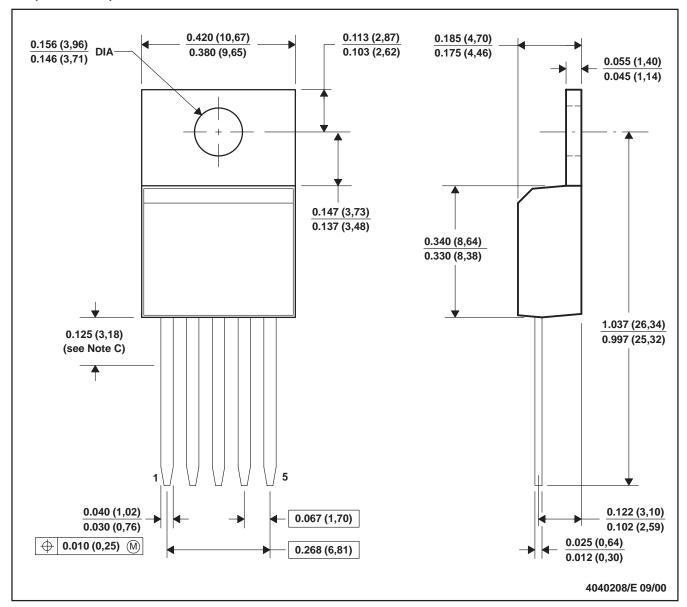


- NOTES:
- A. All linear dimensions are in inches (millimeters).
- B. This drawing is subject to change without notice.
- C. Dimensions do not include mold protrusions, not to exceed 0.006 (0,15).
- Falls within JEDEC TO—263 variation BA, except minimum lead thickness, maximum seating height, and minimum body length.



KC (R-PSFM-T5)

PLASTIC FLANGE-MOUNT



NOTES: A. All linear dimensions are in inches (millimeters).

- B. This drawing is subject to change without notice.
- C. Lead dimensions are not controlled within this area.
- D. All lead dimensions apply before solder dip.
- E. The center lead is in electrical contact with the mounting tab.

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Mailing Address: Texas Instruments

Post Office Box 655303 Dallas, Texas 75265

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